

1 **Assessment of acoustic-mechanical measurements for**
2 **texture of French fries: Comparison of deep-fat frying**
3 **and air frying**

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25 **Abstract**

26 The aim of this study was to develop an instrumental method for measuring the
27 texture of French fries and correlated it with sensory measurements. For seven samples
28 of French fries with different crispness levels, a cone penetrometer test was conducted
29 simultaneously with microphone recording of sound emissions. A descriptive sensory
30 analysis was also performed on these samples. The results showed that the number of
31 sound peaks, the linear distance of sound peaks, the area under the sound-displacement
32 curve and the mean sound pressure were strongly positively correlated ($r \geq 0.80$; P-
33 value < 0.02) with the crispness of the crust descriptor. The number of force peaks and
34 the linear distance of the force peaks were correlated with all the acoustic parameters.
35 These two mechanical parameters and the maximum force, were not correlated with
36 crispness of the crust ($r = 0.50$; P-value < 0.05) but strongly correlated with product
37 hardness ($r = 0.9$; P-value < 0.01). However, the combination of the acoustic and
38 mechanical parameters appeared suitable for measuring the texture of French fries. An
39 analysis of the variable importance by random forest showed that the main parameters
40 for quantifying the texture differences were the number of sound peaks and the
41 maximum force. The use of this instrumental method and sensory analysis showed that
42 the deep-fat fried products were crispier than the air fried products with the same water
43 loss.

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54 **Highlights (maximum 85 characters)**

55 ▶ Combination of acoustic and penetration tests are used to evaluate French fries
56 texture

57 ▶ A high correlation exists between the sensory crispness and the acoustic
58 parameters

59 ▶ The NSP and the Fmax makes it possible to clearly identify the crispness

60 ▶ Deep-fat fried products are crispier than the air fried products with the same
61 water loss

62 **Keywords**

63 French fries; Hot air frying; Texture; Sensory analysis, Crispness; Acoustic properties.
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Abbreviations

Fmax	Maximum force
NFP	Number of force peaks
LDF	Linear distance of force peaks
F_Average	Average drop off of force peaks
Smax	Maximum of sound pressure
MS	Mean of sound pressure
AS	Area under sound displacement curve
NSP	Number of sound peaks
LDS	Linear distance of sound peaks
S_Average	Average dropp off of sound peaks
T	Temperature (°C)
i.m	Initial mass

74 1. Introduction

75 French fries are a specific solid with a moist and soft core and a crispy outer dry
76 crust of approximately 1–2 mm (Bouchon & Aguilera, 2001; Pedreschi & Aguilera,
77 2002; Van Koerten, Schutyser, Somsen, & Boom, 2015). French fries are popular potato
78 products in many countries because of their structure and attractive texture. Texture is
79 one of the important quality aspects, and a crispy crust is a factor in the sensory
80 properties of French fries (Pedreschi & Aguilera, 2002; Salvador, Varela, Sanz, &
81 Fiszman, 2009). Crispness is one of the most important quality parameters in
82 consumers' choice of a fried product (L. M. Duizer, Campanella, & Barnes, 1998;
83 Luyten, Plijter, & Vliet, 2004; Salvador, Varela, Sanz, & Fiszman, 2009; Tunick et al.,
84 2013). Many types of experiments have been conducted to determine crispness, but the
85 best measurements to assess crispness remain to be established (Gondek, Lewicki, &
86 Ranachowski, 2006; Luyten & Vliet, 2006; Castro-Prada, Luyten, Lichtendonk, Hamer,
87 & Vliet, 2007). This sensory attribute is often evaluated by sensory panel tests.
88 Unfortunately, sensory evaluations are expensive, unsuitable for routine testing and
89 generally provide a more qualitative than quantitative comparison (Zdunek, Cybulska,
90 Konopacka, & Rutkowski, 2011). Moreover, the results obtained from different sensory
91 panels are difficult to compare (Roudaut, Dacremont, Vallès Pàmies, Colas, & Le
92 Meste, 2002).

93 Several studies were carried out on the crispness of French fries using mechanical
94 tests (penetration, compression, bending). During a texture analysis, a force can be
95 exercised on a fried sample when a probe moves through it that imitates a first bite of
96 the product. Subsequently, the force-deformation curve is used to calculate the
97 quantitative parameters related to the crust fragility (Miranda & Aguilera, 2006; Van
98 Koerten, Schutyser, Somsen, & Boom, 2015). However, the results of the force-

99 deformation often do not show clearly a correlation with sensory crispness.
100 Nevertheless, [Van Loon \(2005\)](#) showed a correlation between the number of peaks in
101 the force-deformation and sensory perception of crispness of French fries. Instrumental
102 techniques present some advantages, especially in industrial environments in which
103 quick and easy-to-use methods are in great demand and are economically more
104 profitable ([Saeleaw & Schleining, 2011](#)). Other new texture measurement techniques,
105 such as acoustic measurements, have been used on crispy products other than French
106 fries, such as chips, wafer products, and have found high correlations with sensory
107 measurements ([L. Duizer, 2001](#); [Marzec, Cacak-Pietrzak, & Gondek, 2011](#); [Saeleaw,](#)
108 [Dürschmid, & Schleining, 2012](#); [Çarşamba, Duerschmid, & Schleining, 2018](#)). The
109 combination of acoustic and mechanical techniques has been shown to better describe
110 food texture than either of the two techniques alone ([L. Piazza & Giovencana, 2015](#);
111 [Laura Piazza, Gigli, & Ballabio, 2007](#)). The tests, mainly 3-point bending, penetration,
112 and compression methods, predicted the snack crunch ([L. Duizer, 2001](#)) and showed
113 good correlations between the acoustic-mechanical and sensory parameters. Other
114 studies have also shown that the sounds produced during food disintegration play an
115 important role in the perception of the texture of food materials ([L. Duizer, 2001](#);
116 [Luyten & Vliet, 2006](#)). Sometimes these sounds describe the overall quality of a food
117 product better than any other sensory characteristic ([A. marzec, G. cacak-pietrzak & E.](#)
118 [Gondek, 2011](#)). The mechanical (penetration test) and acoustic evaluation of crispness
119 was also used to describe the texture of cookies ([Chen, Karlsson, & Povey, 2005](#)),
120 extruded bread ([Marzec, Lewicki, & Ranachowski, 2007](#)), toasted nuts ([Salvador,](#)
121 [Varela, Sanz, & Fiszman, 2009](#)) and apples ([Zdunek, Cybulska, Konopacka, &](#)
122 [Rutkowski, 2011](#)).

123 The aim of this study was to develop an instrumental method for measuring the
124 texture of French fries, and especially the crispness of the crust. A penetration test was

125 conducted simultaneously with microphone recording of sound emissions. A descriptive
126 sensory analysis was performed to evaluate the textural attributes, and the relationships
127 between the sensory parameters and the instrumental measurement parameters were
128 analysed. Finally, this approach was used to compare two products with contrasting
129 texture made using deep fat frying and air frying.

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131 **2. Materials & Methods**

132 **2.1. Raw materials**

133 The experiments were carried out with frozen French fries (Mc-Cain Tradition)
134 purchased at a local supermarket and stored in a cold room at – 18 °C. The frozen
135 French fries were resized to 60 mm in length and 10 mm thick (10×10×60 mm) with a
136 specific cutter. Each experiment was conducted with 0.300 kg of sized French fries.

137 **2.2. Frying equipment**

138 Two main fryers were used: a commercial oil bath fryer (Filtr One FF162100
139 Seb) with a power of 1900 W, a chip capacity of 1.20 kg and an oil capacity of 2.10 L,
140 and hot-air frying equipment (Airfryer Philips XL HD9240/90, Avance Collection,
141 Amsterdam, The Netherlands) with a power of 2100 W.

142 **2.3. Sample preparation**

143 French fries with different crispness levels were obtained by adapting the frying
144 equipment type, water loss and frying temperature.. Each experiment was carried out
145 with 0.300 kg of sized French fries. Three French fries samples were fried at 180 °C
146 with a conventional deep-fat fryer for final water losses of 60 %, 50 % and 45 %. Four
147 French fries samples were prepared using the hot air fryer. Three of them were fried at
148 140 °C, 180 °C and 200 °C until the water loss reached 50 %. The fourth sample was

149 fried at 180 °C until a water loss of 60 %. The samples were coded according to their
150 frying conditions, as shown in Table 1. All French fries samples were analysed in under
151 5 min. The water loss was defined as the mass of water lost during frying divided by the
152 initial mass (i.m) of the sample before frying.

153 **2.4. Instrumental texture analysis**

154 A penetration test was conducted with a conical probe with a 60° angle.
155 Mechanical (penetration test) and acoustic measurements were made using a texture
156 analyser (TA.XT.plus, Stable Micro Systems (SMS), Surrey, U.K) using a 5 kg sensor
157 connected to a microphone (Brüel Kjaer, Type 2671 Naerum, Denmark). This set was
158 placed in the Thermal Cabinet (TC/LN2 for the TA.XTplus Texture Analyser), which
159 was regulated at 50 °C. The microphone included an acoustic envelope detector (AED)
160 to avoid background noise. It was calibrated with a type 4231 acoustic calibrator (1 Hz,
161 Brüel Kjaer) at 94 and 114 dB sound pressure. The acoustic detector included a sound
162 amplification element that was set to level 2. The microphone position was 1.6 cm from
163 the sample at an angle of 50°. Different test speed (0.2 mm.s⁻¹, 0.5 mm.s⁻¹, 1 mm.s⁻¹
164 and 2 mm.s⁻¹) and deformation level (50 % and 80 %) were tried. The thermal cabinet
165 was turned off during the measurement due to the background noise of its fan. It was
166 used as a partition for the external environmental noise and for the sound emitted by the
167 sample. The conical probe was applied at a position of 20 mm from the extremity of the
168 French fry (1/3 of the length of the French fry). Each French fry was penetrated only
169 once. The measurements were carried out in triplicate with approximately fifteen French
170 fries per test.

171 The following parameters—maximum force (Fmax, N), number of force
172 peaks (NFP), linear force peak distance (LDF, Nm), maximum sound pressure level
173 (Smax, dB), mean of sound pressure (MS, dB), area under the sound displacement
174 curve (AS, dB m), number of sound peaks (NSP), linear distance of sound peaks (LDS,

175 dB m) and average drop-off of sound peaks (F_Average, dB)—were evaluated with the
176 software Exponent (Stable Micro Systems) from the force-deformation curves and
177 acoustic displacement (Figure 1) in a range from 0 to 5 mm corresponding to 50%
178 deformation. The definitions of the instrumental parameters are described in detail
179 elsewhere (Varela, Salvador, & Fiszman, 2008; L. Piazza & Giovenzana, 2015; Kirmaci
180 & Singh, 2016). The sound pressure levels and force-deformation curves were recorded
181 with a detection threshold of 5 dB and 0.05 N, respectively. The same threshold values
182 were used for the detection of the number of sound peaks and the number of force
183 peaks.

184 **2.5. Sensory analysis**

185 *2.5.1. Experimental conditions*

186 A quantitative descriptive analysis (QDA) was used to evaluate the sensory
187 characteristics of the samples. The sensory profiles were performed in the sensory
188 analysis laboratory of the QualiSud UMR (CIRAD, Montpellier). The room is
189 composed of 15 individual boxes including a small sink and an adaptable light. During
190 the tasting sessions, the room temperature and relative humidity were monitored and
191 averaged 22 ± 4 °C and 29 ± 6 %, respectively. Three or four French fries per
192 experimental conditions were presented in monadic form, 1 to 2 minutes after frying, in
193 petri dishes to keep the product warm. The panel consisted of 13 subjects (6 women and
194 7 men) aged 24 to 50 years, who were trained and qualified for sensory analysis
195 (repeatable, homogeneous).

196 *2.5.2. Descriptors*

197 Five descriptors of relevance were selected based on previous studies and
198 considering the purposes of our study. The sensory descriptors studied were crispness of
199 the crust, product hardness, softness of the core, floury of the core and boiled potato

200 taste. The descriptors were evaluated on a continuous scale from the lowest intensity
201 (value 1) to the highest intensity (value 5). The definitions of and evaluation protocols
202 for the sensory descriptors are described in [Table 2](#).

203 **2.5.3. Jury training**

204 Before the tasting started, four training sessions, according to ISO 8586 (2012),
205 were carried out on four types of French fries. These were fried to present the average
206 and extreme intensities of each descriptor. The tasting panel was trained on the different
207 descriptors in the first two training sessions. The last two training sessions were
208 dedicated to assessing the panel's ability to use the descriptors. The scores assigned by
209 the judges were compared to those given by consensus, and judges were asked to
210 comply with the desired benchmark. The jury's training was validated by a statistical
211 analysis, analysing their repeatability. Non-repeatable judges were eliminated for the
212 remainder of the evaluation. Thirteen judges were validated.

213 **2.5.4. Tasting sessions**

214 The seven French fries samples were coded and then submitted to the jury for
215 analysis, giving a score ranging from 1 to 5 for each descriptor out of four tasting
216 sessions. At each tasting session, three to four samples were presented in succession.
217 The order of the samples was determined randomly. The tasting was then carried out in
218 duplicate for each sample.

219 **2.6. Statistical analysis**

220 The statistical analysis of the results was carried out using XLSTAT version 2017
221 (ANOVA and PCA test) and R programs (decision tree test “rpart”). The ANOVA
222 procedure at a significance level at 0.05 and the Tukey test were applied to assess
223 significant differences between the investigated parameters. A correlation analysis
224 (PCA) and a decision tree followed by a random forest were also conducted. An

225 ensemble learner was built on decision trees, in which each decision tree was made with
226 a bagging of observations and instrumental parameters. The mean decrease in accuracy
227 caused by a parameter was determined during the out-of-bag error calculation phase
228 from running the random forest 1000 times (number of trees = 1000, sample size =
229 63%, and no. of variables tried at each split = 2). The parameter importance estimated
230 from the random forest was defined as the percentage of misclassifications.

231 The results of the PCA analysis were presented as a two-dimensional graph: a
232 graph that represents both variables and samples in two dimensions.

233

234 **3. Results and discussion**

235 **3.1. Sensory analysis**

236 The ANOVA's results of the sensory analysis are summarized in [Table 3](#). Seven
237 high-contrast texture samples were generated based on final water loss, frying method
238 and frying temperature. Five sensory descriptors were analysed. The floury of the core
239 was not significantly different for the seven samples. Its value ranged from 1.9 to 3.1.
240 This descriptor is not presented in [Table 3](#). The crispness of the crust, product hardness,
241 softness of the core descriptors and boiled potato taste made it possible to classify the
242 seven samples into 4, 4, 2 and 3 groups, respectively. The variation coefficient of these
243 descriptors in the range from 4 and 10% was satisfactory. It was mainly the crispness of
244 the crust (F-value = 44) and product hardness that differentiate the samples (F-
245 value = 20). This is demonstrated in Figure 2, which presents the bi-plot PCA on
246 covariance, regarding the sensory descriptors data set for the seven French fries
247 samples. The average jury scores for the two tasting sessions are represented in
248 Figure 2. The first two dimensions explain 91.2 % of the variability (56.8 % F1,
249 34.4 % F2). The crispness of the crust and boiled potato taste descriptors contribute
250 highly to the F1 axis respectively 62% and 20%. The product DF180_60 and

251 AY140_50 strongly drives the F1 axis. The axis F2 was more explained by the
252 descriptors softness of the core (39.5 %), floury of the core (32.7 %) and product
253 hardness (23.3 %). There was no correlation between the product hardness and the
254 crispness of the crust ($r = 0.47$; P-value < 0.05). Çarşanba, Duerrschmid, & Schleining
255 (2018) also showed on wafer products that hardness and crispness were also slightly
256 correlated. In addition, the product hardness was strongly negatively correlated with the
257 softness of the core ($r = -0.83$; p-value < 0.02). The crispness of the crust was strongly
258 negatively correlated with only the boiled potato taste ($r = -0.88$; P-value < 0.01). The
259 PCA (Figure 2) shows that the seven French fries samples were repeatable quite varied
260 and well dispersed, thus explaining the different sensory descriptors. Afterwards, these
261 seven samples with contrasting textures were used to characterize the performance of
262 the instrumental measurements of texture.

263 3.2. Instrumental analysis: acoustics and force-deformation test

264 Four different test speeds were used (0.2 mm.s^{-1} , 0.5 mm.s^{-1} , 1 mm.s^{-1} and
265 2 mm.s^{-1}), and two deformation levels (50 % and 80 %). The results showed that the
266 use of a high test speed (2 mm.s^{-1}) did not allow a significant difference between
267 products, but a too low test speed (0.2 mm.s^{-1}) produces high significant differences but
268 with a high variation coefficient (55 %). A moderate test speed of 0.5 mm.s^{-1} was used
269 to make a successful compromise to minimize the variation coefficient. The
270 deformation levels has no significant effect. The deformation level 50 % was used.

271 Figure 1 shows typical force-distance and acoustic amplitude-distance curves for
272 two products: one very crispy and the other slightly crispy. In Figure 1 a), more acoustic
273 and mechanical events were observed than in Figure 1 b). In Figure 1 b), when the force
274 was at a maximum (1.2 N), no acoustic event was observed, whereas in Figure 1 a),

275 when the force was at a maximum (1.4 N), there were more acoustic events. This shows
276 that the two products have different behaviours.

277 The maximum deformation forces did not exceed 5 N with a conical probe. This
278 value was in the same order of magnitude as reported by [Kirmaci and Singh \(2016\)](#) with
279 a penetration probe. The sound pressure level did not exceed 150 dB, which was in the
280 same order of magnitude as those determined by [Çarşamba, Duerrschmid, & Schleining](#)
281 [\(2018\)](#) and [Chen, Karlsson, & Povey \(2005\)](#) on wafer products and biscuits
282 respectively. The sound pressure level was difficult to compare with the literature, as it
283 depended largely on the amplification level and the microphone location with regard to
284 the sample and on the product ([Tunick et al., 2013](#)). In most cases, the sound pressure
285 level ranged from 60 dB to 90 dB ([Sanz, Primo-Martín, & van Vliet, 2007](#); [Saeleaw et](#)
286 [al., 2012](#); [Çarşamba, Duerrschmid, & Schleining, 2018](#)) for a crispy product.

287 These profiles (acoustic-distance and force-distance) made it possible to retrieve
288 the mechanical (penetration test) and acoustic parameters. All the experimental results
289 are gathered in [Table 3](#) with an ANOVA (p -value < 0.05). Four mechanical (penetration
290 test) parameters were analysed, including the average drop-off of force peaks, which did
291 not allow any significant difference between the seven products. Thus, it will not be
292 discussed later. The number of force peaks (NFP) separated the samples into four
293 different groups. This parameter ranged from 13.3 to 1.9 among groups with a relative
294 uncertainty smaller than 25 %. The maximum force (Fmax) and linear distance of force
295 peaks (LDF) separated the samples in the same way. These parameters made it possible
296 to distinguish two product groups. For the LDF and Fmax parameters, the variation
297 ranges were 5.9 N m to 19.8 N m and 1.3 N to 4.3 N, respectively. The relative
298 uncertainty of these two parameters ranged from 4 to 20%. The number of force peaks
299 (NFP; F-value = 32.13) was more discriminating and provides different information
300 compared to Fmax (F-value = 30.71) and LDF (F-value = 19.3).

301 The analysis of the acoustic parameters showed that the number of sound
302 peaks (NSP) and the linear distance of sound peaks (LDS) followed the same rankings
303 by significantly separating the products into five different groups. The area under the
304 sound displacement curve (AS) and the mean of the sound pressure (MS) parameters
305 also grouped the samples in the same way by classifying them into four product groups.
306 For this reason, the area under the sound displacement curve (AS) was not presented in
307 [Table 3](#). The relative uncertainty of these parameters ranged from 7 to 20 % for NSP (F-
308 value = 60.7) and LDS (F-value = 58.3) and from 7 to 35 % for AS (F-value = 46.6) and
309 MS (F-value = 46.7). The maximum sound pressure (Smax) allowed the separation of
310 the products into four groups with both a low relative uncertainty ($< 7\%$) and a low
311 variation amplitude (75 to 50) when compared to the other acoustic parameters, such as
312 NSP (87 to 7) and MS (10.5 to 0.5). By comparing the F-value of these acoustic
313 parameters, it can be observed that the Smax has a lower F-value (Smax, F-value = 23)
314 compared to the other parameters. The low F-value and low variation amplitude can
315 lead to a lack of efficiency of this parameter to detect significant differences when the
316 products to compare have a low texture difference.

317 The various acoustic parameters can be split into three groups (NSP/LDS, Smax
318 and AS/MS), and the mechanical (penetration test) parameters into two groups (NFP
319 and Fmax/LDF). The acoustic parameters separated the products into at least four
320 groups with high F-value, while the mechanical parameters allowed their classification
321 into two and four maximum groups with lower F-value than acoustic parameters.
322 Therefore, the acoustic parameters are more sensitive than the penetration test
323 parameters.

324 The analysis of the different confidence intervals and different F-values showed
325 that mechanical responses were more repeatable (3 to 18 % relative uncertainty) but
326 were less discriminating (low F-value) than acoustic responses (5 to 25 % relative

327 uncertainty). It is important to point out that the experimental variance was determined
328 with approximately forty-five values (French fries measured). This result shows that
329 this instrumental measurement was not as simple to carry out and required careful
330 implementation conditions to be reproducible.

331 **3.3. Correlation between the results of instrumental and sensory analysis**

332 Figure 3 shows a PCA on correlation, performed to illustrate the relation between
333 some mechanical (penetration test) and acoustic parameters and sensory descriptors of
334 French fries. The PCA showed that 87.60 % of the variability could be explained by the
335 first two main components: 69.76 % by the first component F1 and 17.84 % by the
336 second component F2. Instrumental parameters were projected as supplementary
337 variables and did not influence on the principal components of the analysis. The first
338 dimension (F1 axis) is particularly linked to the variables product hardness (29 %),
339 boiled potato taste (29 %), crispiness of the crust (27 %) and softness of the core (15%).
340 The second axis is more related to the floury of the core (48 %) and the softness of the
341 core (20 %). This bi-plot illustrates that the products DF180_60 and DF180_50 were
342 associated with higher values of the acoustic parameters. These products were the
343 crispiest by sensory analysis. The AY180_60 product, which was considered harder and
344 moderately crispy, was associated with higher values of Fmax and product hardness.
345 The products AY40_50, AY180_50 and AY200_50 were characterized by lower values
346 of most of the acoustic parameters but were associated with higher values of boiled
347 potato taste. These products had the lowest crispness scores and were, therefore,
348 considered less crispy by the sensory analysis. Therefore, it can be concluded that an
349 increase in acoustic parameters reflects a high level of crispness. This is in line with
350 several previous works ([Saeleaw & Schleining, 2011](#); [Giacosa et al., 2016](#); [Jakubczyk,
351 Gondek, & Tryzno, 2017](#); [Çarşamba, Duerrschmid, & Schleining, 2018](#)).

352 Some instrumental parameters were more or less correlated with each other, unlike
353 sensory parameters, which were distinct from each other (Figure 3). Most of the
354 acoustic parameters studied were positively correlated with each other, except for
355 the S_Average which was more closely related to the F2 axis. The acoustic parameters
356 NSP ($r = 0.89$; P-value < 0.01), LDS ($r = 0.90$; P-value < 0.01), Smax ($r = 0.94$; P-
357 value < 0.01) and MS ($r = 0.89$; P-value < 0.01) were strongly positively correlated with
358 the crispness of the crust, with a high level of significance (Table 4). According to this,
359 a small number of acoustic events was considered as an indication of a low crispness of
360 the crust. This conclusion is in line with the work of Salvador, Varela, Sanz, & Fiszman
361 (2009), who obtained the same conclusion with potato chips. Smax, NSP and MS were
362 specifically used to explain the crispness and crunchiness of extruded snacks by
363 Saeleaw and Schleining (2011). In contrast, the sensory descriptor boiled potato taste
364 was negatively correlated to all these parameters (Figure 3). The crispier the products
365 were, the less the products taste like boiled potatoes.

366 The mechanical (penetration test) parameters were not significantly correlated with
367 the crispness of the crust for P-value < 0.05 (LDF $r = 0.70$, P-value > 0.05 ;
368 F_max $r = 0.5$, P-value > 0.05), except for the NFP parameter ($r = 0.84$; P-
369 value < 0.05). In contrast, F max was strongly correlated with the product
370 hardness ($r = 0.9$; P-value < 0.01). Obviously, the descriptor product hardness was not
371 only associated with the mechanical parameters. These results are in line with the work
372 carried out by Jakubczyk, Gondek, & Tryzno (2017) on co-extruded snacks. The
373 sensory descriptor softness of the core was negatively correlated to
374 F max ($r = -0.79$; P-value < 0.05) but not significant for the other instrumental
375 parameters. The harder the products were, the less soft the core was.

376 The relation between the parameters highly correlated with some evaluated sensory
377 texture descriptors was established by analysing the linear regression

378 coefficients (Figure 5). The coefficient of determination (R^2) shows how the
379 instrumental parameters such as NSP and Fmax explain sensory descriptors (crispness
380 of the crust, product hardness, softness of the core or floury of the core) by a linear
381 model. The parameters NSP ($R^2 = 0.80$) shows a high and positive regression coefficient
382 for the sensory crispness of the crust. This instrumental parameter allowed the
383 prediction of the sensory crispness of French fries correctly with high robustness. The
384 coefficient of determination of Fmax relative to hardness was high and reflects a strong
385 correlation between hardness and F max ($R^2 = 0.80$). No parameter can significantly
386 predict the soft and floury of the core. This confirms that the two parameters (NSP and
387 Fmax) reflect the crispness and the product hardness. These results confirm that the two
388 methods provide different and complementary information. The mechanical parameters
389 had better explain the hardness of the product and the softness of the core, and the
390 acoustic parameters better explain the crispness of the crust. The combination of the
391 acoustic and mechanical (penetration test) methods seems appropriate to describe the
392 texture of French fries. Several other previous studies have reported the same
393 conclusion for other crispy food such as dutch crisbakes, wafers, crispy bakery products
394 (Mohamed, Jowitt, & Brennan, 1982; Laura Piazza, Gigli, & Ballabio, 2007; L. Piazza
395 & Giovenzana, 2015).

396 A random forest classification was carried out by comparing 45 deep-fat
397 fries (DF180_50) and 45 hot-air fries (AY180_50). The purpose was to detect the
398 importance of the variables in predicting the class of the French fries (between deep-fat
399 and hot-air). The products were made at the same frying temperature (180 °C) and with
400 the same water loss (50%). Figure 4 a) presents the classification tree relating the frying
401 process groups (deep-fat frying; air frying) to the instrumental parameters. The
402 parameter importance estimated from the random forest was defined as the percentage
403 of misclassifications. The more the accuracy of the random forest decreased due to the

404 exclusion (or permutation) of a single parameter, the more important that parameter was
405 deemed, and therefore, parameters with a large mean decrease in accuracy were more
406 important for the classification of the data. The acoustic parameters were more
407 important, especially the number of sound peaks (NSP) and the linear distance of sound
408 peaks (LDS), followed by the mean sound pressure (MS) and the area under the sound
409 displacement curve (AS). The parameters that have less weight were S_max and NFP.
410 Figure 4 b) shows a good discrimination of the products due to the parameters NSP and
411 Fmax and with an out-of-bag error of just 8.04 %. This confirms the relevance of
412 combining the acoustic parameters with NSP and the mechanical parameters with Fmax
413 with a performance error of 6.6 %. Other important instrumental parameters, such as
414 LDS, MS and AS, did not appear in the classification because they were highly
415 correlated with NSP and with each other. The combination of NSP and Fmax provides a
416 better classification of products. These results confirm also that a minimum hardness
417 (F max) was required to detect the crispness of French fries.

418 **3.4. Impact of frying process on the texture**

419 The analysis of Figure 1 showed that more acoustic and mechanical (penetration
420 test) events were observed for the deep-fat fried products curve (Figure 1 a) than for the
421 air-fried products (Figure 1 b). [Teruel et al. \(2015\)](#) also showed previously that the
422 deep-fat fried fries are crispier than the air-fried fries.

423 **3.4.1. Effect of water loss**

424 Three groups of French fries were generated according to their final water loss,
425 ranging from 45 % to 60 %. An analysis of the sensory parameters did not make it
426 possible to distinguish these three groups according to water loss. Only the Fmax, which
427 reflects the hardness of the product, separated the samples into two groups. In the first
428 group, all samples have a water loss of 60 %, and in the second group, the samples have

429 a final water loss of 45 % and 50 %. The more water was lost, the harder the product
430 became. For the other instrumental parameters, the effect of water loss was more
431 difficult to detect because of the combination of effects of process, temperature and
432 water loss. Indeed, it was possible to obtain the same water loss with different operating
433 conditions, and it was the rate of water transfer that was probably more important for
434 the texture of the product (Vitrac, Trystram, & Raoult-Wack, 2000; Bouchon &
435 Aguilera, 2001; Botero-Uribe, Fitzgerald, Gilbert, & Midgley, 2017). However, the
436 analysis of samples performed with deep-fat frying at 180 °C showed that an increase in
437 water loss increased the crispness of the crust and the product hardness. In contrast, the
438 softness of the core decreased with the water loss. In the instrumental parameters, there
439 was also an increase in mechanical and acoustic events as a function of water loss. For
440 comparing crispy products, it could be especially important to consider the water
441 content of the product (Seymour & Ann, 1988; Saeleaw, Dürschmid, & Schleining,
442 2012)

443 *3.4.2. Effect of air temperature*

444 An analysis of the air-fried samples with the same water loss of 50 % showed that
445 an increase in frying temperature from 140 °C to 180 °C or 200 °C increased the values
446 of the crispness of the crust and product hardness. This is in line with several previous
447 works (Kita, Lisińska, & Gołubowska, 2007; van Koerten et al., 2015). The acoustic
448 parameter values also increased as the frying temperature increased. From 180 °C to
449 200 °C, the increase in the values of the various instrumental parameters analysed was
450 not significant. These results confirm the conclusions of van Koerten, Schutyser,
451 Somsen, & Boom (2015) that state that increased frying temperatures will improve the
452 crispy properties of the fries due to the formation of more and larger pores, but this
453 improvement only occurs until the temperature reaches a certain maximum, which was
454 between 180 and 195 °C. The sample (AY140_50) obtained by air frying at 140 °C has

455 the lowest values of crispness of the crust and product hardness but has the highest
456 value of softness at the core. The low air frying temperature (140 °C) was not sufficient
457 to develop a crispy crust, such as that developed at temperatures of 180 °C and 200 °C.
458 This difference is due to the low heat and mass transfer rates, which are responsible for
459 the development of the particular texture of fried products. ([Loon, 2005](#); [Kita, Lisińska,](#)
460 [& Gołubowska, 2007](#); [Thussu & Datta, 2012](#); [Zeb, 2019](#)).

461

462

463 4. Conclusion

464 This study allowed the development of an instrumental method for measuring the
465 texture of French fries. The penetration test and acoustic signals provide different and
466 complementary information. Acoustic signals are very sensitive to the crispness of the
467 crust of French fries. Acoustic parameters, such as the number of sound peaks (NPS),
468 the linear distance of sound peaks (LDS), the maximum sound pressure (Smax), the
469 mean sound pressure (MS) and the area under the sound displacement curve (AS), are
470 highly correlated with the sensory crispness of the crust. The instrumental parameters
471 NSP, Smax and the maximum force (Fmax) are suitable for good characterization of the
472 texture of French fries, especially the crispness of the crust and the product hardness.
473 By using a combination of mechanical (penetration test) and acoustic approaches, it was
474 possible to better estimate the texture of French fries than by using one of the other
475 technique alone.

476 However, this method requires a large number of repetitions (about thirty French
477 fries) and requires careful implementation conditions to be reproducible. The
478 instrumental tests were able to evaluate, discriminate and reasonably predict the sensory
479 crispness of the crust of French fries, with an R^2 close to 0.8. In addition, the following
480 specific advantages make this approach suitable for industrial application.

481 The use of this instrumental method and sensory analysis showed that the deep-fat
482 fried products are crispier than the air fried products and that water loss has an effect on
483 the crispness and hardness of the fries. It is important to take into account the moisture
484 content when comparing the crispness or hardness of fried products.

485

486 **5. Acknowledgements**

487 This study was funded by SEB Group, ANRT and CIRAD-Montpellier. We would like
488 to express our thanks to Baptiste Graglia, an engineering student from the University of
489 Montpellier, as well as to the sensory analysis laboratory of the CIRAD Montpellier for
490 their valuable collaboration, and Ricci Julien, Laboratory Technician at QualiSud UMR,
491 for his assistance.

492

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494 **6. References**

495 Botero-Uribe, M., Fitzgerald, M., Gilbert, R. G., & Midgley, J. (2017). Effect of pulsed
496 electrical fields on the structural properties that affect french fry texture during
497 processing. *Trends in Food Science & Technology*, 67, 1–11.

498 <https://doi.org/10.1016/j.tifs.2017.05.016>

499 Bouchon, P., & Aguilera, J. M. (2001). Microstructural analysis of frying potatoes.

500 *International Journal of Food Science & Technology*, 36(6), 669–676.

501 <https://doi.org/10.1046/j.1365-2621.2001.00499.x>

502 Çarşamba, E., Duerrschmid, K., & Schleining, G. (2018). Assessment of acoustic-

503 mechanical measurements for crispness of wafer products. *Journal of Food*

504 *Engineering*, 229, 93–101. <https://doi.org/10.1016/j.jfoodeng.2017.11.006>

505 Castro-Prada, E. M., Luyten, H., Lichtendonk, W., Hamer, R. J., & Vliet, T. V. (2007).

506 An Improved Instrumental Characterization of Mechanical and Acoustic

507 Properties of Crispy Cellular Solid Food. *Journal of Texture Studies*, 38(6),
508 698–724. <https://doi.org/10.1111/j.1745-4603.2007.00121.x>

509 Chen, J., Karlsson, C., & Povey, M. (2005). Acoustic Envelope Detector for Crispness
510 Assessment of Biscuits. *Journal of Texture Studies*, 36(2), 139–156.
511 <https://doi.org/10.1111/j.1745-4603.2005.00008.x>

512 Duizer, L. (2001). A review of acoustic research for studying the sensory perception of
513 crisp, crunchy and crackly textures. *Trends in Food Science & Technology*,
514 12(1), 17–24. [https://doi.org/10.1016/S0924-2244\(01\)00050-4](https://doi.org/10.1016/S0924-2244(01)00050-4)

515 Duizer, L. M., Campanella, O. H., & Barnes, G. R. G. (1998). Sensory, Instrumental
516 and Acoustic Characteristics of Extruded Snack Food Products. *Journal of*
517 *Texture Studies*, 29(4), 397–411. [https://doi.org/10.1111/j.1745-](https://doi.org/10.1111/j.1745-4603.1998.tb00812.x)
518 [4603.1998.tb00812.x](https://doi.org/10.1111/j.1745-4603.1998.tb00812.x)

519 Giacosa, S., Belviso, S., Bertolino, M., Dal Bello, B., Gerbi, V., Ghirardello, D., ...
520 Rolle, L. (2016). Hazelnut kernels (*Corylus avellana* L.) mechanical and
521 acoustic properties determination: Comparison of test speed, compression or
522 shear axis, roasting, and storage condition effect. *Journal of Food Engineering*,
523 173, 59–68. <https://doi.org/10.1016/j.jfoodeng.2015.10.037>

524 Gondek, E., Lewicki, P. P., & Ranachowski, Z. (2006). Influence of Water Activity on
525 the Acoustic Properties of Breakfast Cereals. *Journal of Texture Studies*, 37(5),
526 497–515. <https://doi.org/10.1111/j.1745-4603.2006.00065.x>

527 Jakubczyk, E., Gondek, E., & Tryzno, E. (2017). Application of novel acoustic
528 measurement techniques for texture analysis of co-extruded snacks. *LWT*, 75,
529 582–589. <https://doi.org/10.1016/j.lwt.2016.10.013>

530 Kirmaci, B., & Singh, R. K. (2016). Quality of the pre-cooked potato strips processed
531 by Radiant Wall Oven. *LWT - Food Science and Technology*, 66, 565–571.
532 <https://doi.org/10.1016/j.lwt.2015.11.006>

- 533 Kita, A., Lisińska, G., & Gołubowska, G. (2007). The effects of oils and frying
534 temperatures on the texture and fat content of potato crisps. *Food Chemistry*,
535 102(1), 1–5. <https://doi.org/10.1016/j.foodchem.2005.08.038>
- 536 Loon, W. a. M. (2005). *Process innovation and quality aspects of French fries*.
537 Retrieved from [http://agris.fao.org/agris-](http://agris.fao.org/agris-search/search.do?recordID=NL2012023842)
538 [search/search.do?recordID=NL2012023842](http://agris.fao.org/agris-search/search.do?recordID=NL2012023842)
- 539 Luyten, H., Plijter, J. J., & Vliet, T. V. (2004). Crispy/Crunchy Crusts of Cellular Solid
540 Foods: A Literature Review with Discussion. *Journal of Texture Studies*, 35(5),
541 445–492. <https://doi.org/10.1111/j.1745-4603.2004.35501.x>
- 542 Luyten, H., & Vliet, T. V. (2006). Acoustic Emission, Fracture Behavior and
543 Morphology of Dry Crispy Foods: A Discussion Article. *Journal of Texture*
544 *Studies*, 37(3), 221–240. <https://doi.org/10.1111/j.1745-4603.2006.00049.x>
- 545 Marzec, A., Cacak-Pietrzak, G., & Gondek, E. (2011). Mechanical and Acoustic
546 Properties of Spring Wheat Versus Its Technological Quality Factors. *Journal of*
547 *Texture Studies*, 42(4), 319–329. [https://doi.org/10.1111/j.1745-](https://doi.org/10.1111/j.1745-4603.2011.00284.x)
548 [4603.2011.00284.x](https://doi.org/10.1111/j.1745-4603.2011.00284.x)
- 549 Marzec, A., Lewicki, P. P., & Ranachowski, Z. (2007). Influence of water activity on
550 acoustic emission of flat extruded bread. *Journal of Food Engineering*, 79(2),
551 410–422. <https://doi.org/10.1016/j.jfoodeng.2006.01.067>
- 552 Miranda, M. L., & Aguilera, J. M. (2006). Structure and Texture Properties of Fried
553 Potato Products. *Food Reviews International*, 22(2), 173–201.
554 <https://doi.org/10.1080/87559120600574584>
- 555 Mohamed, A. A. A., Jowitt, R., & Brennan, J. G. (1982). Instrumental and sensory
556 evaluation of crispness: I—In friable foods. *Journal of Food Engineering*, 1(1),
557 55–75. [https://doi.org/10.1016/0260-8774\(82\)90013-9](https://doi.org/10.1016/0260-8774(82)90013-9)

- 558 Pedreschi, F., & Aguilera, J. M. (2002). Some Changes in Potato Chips During Frying
559 Observed by Confocal Laser Scanning Microscopy (CLSM). *Food Science and*
560 *Technology International*, 8(4), 197–201.
561 <https://doi.org/10.1106/108201302027931>
- 562 Piazza, L., & Giovenzana, V. (2015). Instrumental acoustic-mechanical measures of
563 crispness in apples. *Food Research International*, 69, 209–215.
564 <https://doi.org/10.1016/j.foodres.2014.12.041>
- 565 Piazza, Laura, Gigli, J., & Ballabio, D. (2007). On the application of chemometrics for
566 the study of acoustic-mechanical properties of crispy bakery products.
567 *Chemometrics and Intelligent Laboratory Systems*, 86(1), 52–59.
568 <https://doi.org/10.1016/j.chemolab.2006.08.005>
- 569 Piazza, Laura, Gigli, J., & Ballabio, D. (2007b). On the application of chemometrics for
570 the study of acoustic-mechanical properties of crispy bakery products.
571 *Chemometrics and Intelligent Laboratory Systems*, 86(1), 52–59.
572 <https://doi.org/10.1016/j.chemolab.2006.08.005>
- 573 Roudaut, G., Dacremont, C., Vallès Pàmies, B., Colas, B., & Le Meste, M. (2002).
574 Crispness: A critical review on sensory and material science approaches. *Trends*
575 *in Food Science & Technology*, 13(6), 217–227. [https://doi.org/10.1016/S0924-](https://doi.org/10.1016/S0924-2244(02)00139-5)
576 [2244\(02\)00139-5](https://doi.org/10.1016/S0924-2244(02)00139-5)
- 577 Saeleaw, M., Dürschmid, K., & Schleining, G. (2012). The effect of extrusion
578 conditions on mechanical-sound and sensory evaluation of rye expanded snack.
579 *Journal of Food Engineering*, 110(4), 532–540.
580 <https://doi.org/10.1016/j.jfoodeng.2012.01.002>
- 581 Saeleaw, M., Dürschmid, K., & Schleining, G. (2012). The effect of extrusion
582 conditions on mechanical-sound and sensory evaluation of rye expanded snack.

583 *Journal of Food Engineering*, 110(4), 532–540.
584 <https://doi.org/10.1016/j.jfoodeng.2012.01.002>

585 Saeleaw, M., & Schleining, G. (2011). A review: Crispness in dry foods and quality
586 measurements based on acoustic–mechanical destructive techniques. *Journal of*
587 *Food Engineering*, 105(3), 387–399.
588 <https://doi.org/10.1016/j.jfoodeng.2011.03.012>

589 Salvador, A., Varela, P., Sanz, T., & Fiszman, S. M. (2009). Understanding potato chips
590 crispy texture by simultaneous fracture and acoustic measurements, and sensory
591 analysis. *LWT - Food Science and Technology*, 42(3), 763–767.
592 <https://doi.org/10.1016/j.lwt.2008.09.016>

593 Salvador, A., Varela, P., Sanz, T., & Fiszman, S. M. (2009). Understanding potato chips
594 crispy texture by simultaneous fracture and acoustic measurements, and sensory
595 analysis. *LWT - Food Science and Technology*, 42(3), 763–767.
596 <https://doi.org/10.1016/j.lwt.2008.09.016>

597 Sanz, T., Primo-Martín, C., & van Vliet, T. (2007). Characterization of crispness of
598 French fries by fracture and acoustic measurements, effect of pre-frying and
599 final frying times. *Food Research International*, 40(1), 63–70.
600 <https://doi.org/10.1016/j.foodres.2006.07.013>

601 Seymour, S. K., & Ann, D. D. H. (1988). Crispness and Crunchiness of Selected Low
602 Moisture Foods¹. *Journal of Texture Studies*, 19(1), 79–95.
603 <https://doi.org/10.1111/j.1745-4603.1988.tb00926.x>

604 Teruel, M. del R., Gordon, M., Linares, M. B., Garrido, M. D., Ahromrit, A., &
605 Niranjana, K. (2015). A Comparative Study of the Characteristics of French Fries
606 Produced by Deep Fat Frying and Air Frying. *Journal of Food Science*, 80(2),
607 E349–E358. <https://doi.org/10.1111/1750-3841.12753>

608 Thussu, S., & Datta, A. K. (2012). Texture prediction during deep frying: A mechanistic
609 approach. *Journal of Food Engineering*, *108*(1), 111–121.
610 <https://doi.org/10.1016/j.jfoodeng.2011.07.017>

611 Tunick, M. H., Onwulata, C. I., Thomas, A. E., Phillips, J. G., Mukhopadhyay, S.,
612 Sheen, S., ... Cooke, P. H. (2013). Critical Evaluation of Crispy and Crunchy
613 Textures: A Review. *International Journal of Food Properties*, *16*(5), 949–963.
614 <https://doi.org/10.1080/10942912.2011.573116>

615 van Koerten, K. N., Schutyser, M. A. I., Somsen, D., & Boom, R. M. (2015). Crust
616 morphology and crispness development during deep-fat frying of potato. *Food*
617 *Research International*, *78*, 336–342.
618 <https://doi.org/10.1016/j.foodres.2015.09.022>

619 Van Loon, W. A. M. (2005). Process innovation and quality aspects of French fries. PhD
620 Thesis Wageningen University, The Netherlands.

621
622 Varela, P., Salvador, A., & Fiszman, S. M. (2008). Methodological developments in
623 crispness assessment: Effects of cooking method on the crispness of crusted
624 foods. *LWT - Food Science and Technology*, *41*(7), 1252–1259.
625 <https://doi.org/10.1016/j.lwt.2007.08.008>

626 Vitrac, O., Trystram, G., & Raoult-Wack, A.-L. (2000). Deep-fat frying of food: Heat
627 and mass transfer, transformations and reactions inside the frying material.
628 *European Journal of Lipid Science and Technology*, *102*(8–9), 529–538.
629 [https://doi.org/10.1002/1438-9312\(200009\)102:8/9<529::AID-](https://doi.org/10.1002/1438-9312(200009)102:8/9<529::AID-EJLT529>3.0.CO;2-F)
630 [EJLT529>3.0.CO;2-F](https://doi.org/10.1002/1438-9312(200009)102:8/9<529::AID-EJLT529>3.0.CO;2-F)

631 Zdunek, A., Cybulska, J., Konopacka, D., & Rutkowski, K. (2011). Evaluation of apple
632 texture with contact acoustic emission detector: A study on performance of
633 calibration models. *Journal of Food Engineering*, *106*(1), 80–87.
634 <https://doi.org/10.1016/j.jfoodeng.2011.04.011>

635 Zeb, A. (2019). *Food Frying: Chemistry, Biochemistry, and Safety*. John Wiley & Sons.

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Table 1: French fries samples condition obtained by deep fat frying (DF) or air frying (AY) at three different temperatures (for oil bath or air) and three different water loss level.

Sample's code	Frying equipment	T (°C)	Water loss (% i.m.)
DF180_60	Deep-fat fryer	180	60
DF180_50	Deep-fat fryer	180	50
DF180_45	Deep-fat fryer	180	45
AY180_60	Air fryer	180	60
AY200_50	Air fryer	200	50
AY180_50	Air fryer	180	50
AY140_50	Air fryer	140	50

Table 2: Definition and evaluation protocol of sensory descriptors

Sensory descriptors	Definition	Evaluation protocol	scoring scale
Crispness of the crust	Mechanical property related to the force required for the surface of the French fries to crumble or break during mastication	Put a French fry in the mouth and evaluate the force required to break the crust	1: Cardboardy 5: Crispy
Product hardness	Ability of the product to resist mechanical strain	Put a French fry in the mouth and evaluate the force required to break the whole French fry.	1: Soft 5: Hard
Softness of the core	Mechanical property related to the force required to obtain a deformation of the core of the French fries during mastication	Evaluate the force required to deform the product by compressing the core of the French fries between the teeth or between the tongue and the palate.	1: Hard 5: Soft
Floury of the core	Mechanical property related to the cohesion and presence of fine particles in the core of French fries during mastication	Put a French fry in the mouth and evaluate the presence of floury particles during mastication	1: Smooth 5: Floury
Boiled potato taste	Aroma of potato cooked in boiling water	Evaluate the intensity of the boiled potato aroma when tasting the French fries	1: Low 5: High

Table 3: Results of sensory analysis and instrumental tests for French fries samples obtained by deep fat frying (DF) or air frying (AY) at three different temperatures (140, 180 and 200 °C) and three different water loss level 45, 50 and 60 (% i.m).

Sample's code	Sensory descriptors				Mechanical test*			Acoustic test**			
	Crispness of the crust	Product hardness	Softness of the core	Boiled potato taste	NFP	LDF (10 ⁻³ N m)	Fmax (N)	NSP	LDS (10 ⁻³ dB m)	Smax (dB)	MS (dB)
DF180_60	4.9 ± 0.2 ^a	3.5 ± 0.3 ^b	3.3 ± 0.3 ^b	1.9 ± 0.2 ^c	13.3 ± 3.5 ^a	19.8 ± 3.7 ^a	3.4 ± 0.6 ^a	87.1 ± 10.4 ^a	6.9 ± 1.3 ^a	75.3 ± 3.5 ^a	10.4 ± 2.3 ^a
DF180_50	4.7 ± 0.3 ^a	2.9 ± 0.3 ^c	4.5 ± 0.2 ^a	2.6 ± 0.3 ^b	7.5 ± 1.0 ^c	9.2 ± 0.5 ^b	1.8 ± 0.2 ^b	54.0 ± 4.5 ^{bc}	4.4 ± 0.7 ^{bc}	69.2 ± 2.5 ^a	5.6 ± 0.5 ^{bc}
DF180_45	3.9 ± 0.3 ^b	3.0 ± 0.2 ^c	4.5 ± 0.2 ^a	2.4 ± 0.5 ^b	4.7 ± 0.7 ^{cd}	7.0 ± 0.3 ^b	1.4 ± 0.2 ^b	39.7 ± 3.1 ^c	3.3 ± 0.3 ^c	67.4 ± 3.8 ^b	3.8 ± 0.3 ^c
AY180_60	3.8 ± 0.4 ^b	4.2 ± 0.2 ^a	3.0 ± 0.3 ^b	2.7 ± 0.5 ^b	9.9 ± 1.3 ^{bc}	15.0 ± 4.5 ^a	4.3 ± 0.6 ^a	66.4 ± 9.3 ^b	5.3 ± 1.2 ^b	70.8 ± 3.3 ^b	6.5 ± 1.8 ^b
AY200_50	3.1 ± 0.3 ^c	3.2 ± 0.2 ^{bc}	3.5 ± 0.3 ^b	2.6 ± 0.3 ^b	2.9 ± 0.7 ^d	6.3 ± 0.4 ^b	1.4 ± 0.2 ^b	20.7 ± 4.1 ^d	1.6 ± 0.2 ^d	59.0 ± 3.2 ^c	1.6 ± 0.5 ^d
AY180_50	3.2 ± 0.2 ^c	3.0 ± 0.2 ^c	4.1 ± 0.2 ^a	2.8 ± 0.3 ^b	2.9 ± 0.7 ^d	6.2 ± 1.2 ^b	1.3 ± 0.2 ^b	16.7 ± 3.5 ^d	1.3 ± 0.2 ^d	57.4 ± 2.6 ^{cd}	1.2 ± 0.3 ^d
AY140_50	2.4 ± 0.3 ^d	2.4 ± 0.3 ^d	4.3 ± 0.2 ^a	3.6 ± 0.2 ^a	1.9 ± 0.4 ^d	5.9 ± 0.2 ^b	1.3 ± 0.3 ^b	6.9 ± 1.7 ^e	0.5 ± 0.1 ^e	50.8 ± 3.5 ^d	0.5 ± 0.2 ^d

Values are the mean ± 95% confidence interval ($n = 26$ (2 tasting sessions × 13 judges) for sensory analysis; $35 \leq n \leq 45$ for acoustical and mechanical analysis).

Means with the same superscript (a–e) within the same column do not differ significantly (Tukey test, p -value ≤ 0.05).

* NFP: number of force peaks; LDF: linear distance of force peaks; Fmax : maximum force

** NSP number of sound peaks; LDS: linear distance of sound peaks; Smax : maximum sound pressure level; MS: mean of sound pressure level

Table 4: Matrix of correlation coefficients (*r*) between investigated variables.

Variables		Sensory descriptors					Mechanical parameters			Acoustic parameters				
		Crispness of the crust	Product hardness	Softness of the core	Floury of the core	boiled potato taste	NFP	LDF	F max	NSP	LDS	Smax	SAire	MS
Sensory descriptors	Crispness of the crust	1*												
	Product hardness	0.47	1*											
	Softness of the core	-0.12	-0.83*	1*										
	Floury of the core	-0.46	0.43	-0.51	1*									
	boiled potato taste	-0.88*	-0.54	0.35	0.43	1*								
Mechanical parameters	NFP	0.84*	0.70	-0.54	-0.09	-0.76	1*							
	LDF	0.70	0.72	-0.66	0.04	-0.68	0.97*	1*						
	F max	0.50	0.89*	-0.79	0.39	-0.44	0.85*	0.89*	1*					
Acoustic parameters	NSP	0.89*	0.71	-0.49	-0.10	-0.81*	0.99*	0.93*	0.81*	1*				
	LDS	0.90*	0.70	-0.47	-0.11	-0.81*	0.99*	0.92*	0.80*	1*	1*			
	Smax	0.94*	0.69	-0.37	-0.16	-0.87*	0.91*	0.81*	0.70	0.96*	0.97*	1*		
	SAire	0.89*	0.64	-0.46	-0.16	-0.81*	0.99*	0.95*	0.77	0.99*	0.99*	0.94*	1*	
	MS	0.89*	0.64	-0.46	-0.16	-0.81*	0.99*	0.95*	0.77	0.99*	0.99*	0.94*	1*	1*

The values of the correlation coefficients are different from 0 with a significance level $\alpha = 0.95$

Values marked with an asterisk (*) correspond to correlation coefficients ≥ 0.8 indicating a high correlation.

NFP: number of force peaks; LDF: linear distance of force peaks; Fmax: maximum force

NSP number of sound peaks; LDS: linear distance of sound peaks; Smax: maximum sound pressure level; MS: mean of sound pressure level

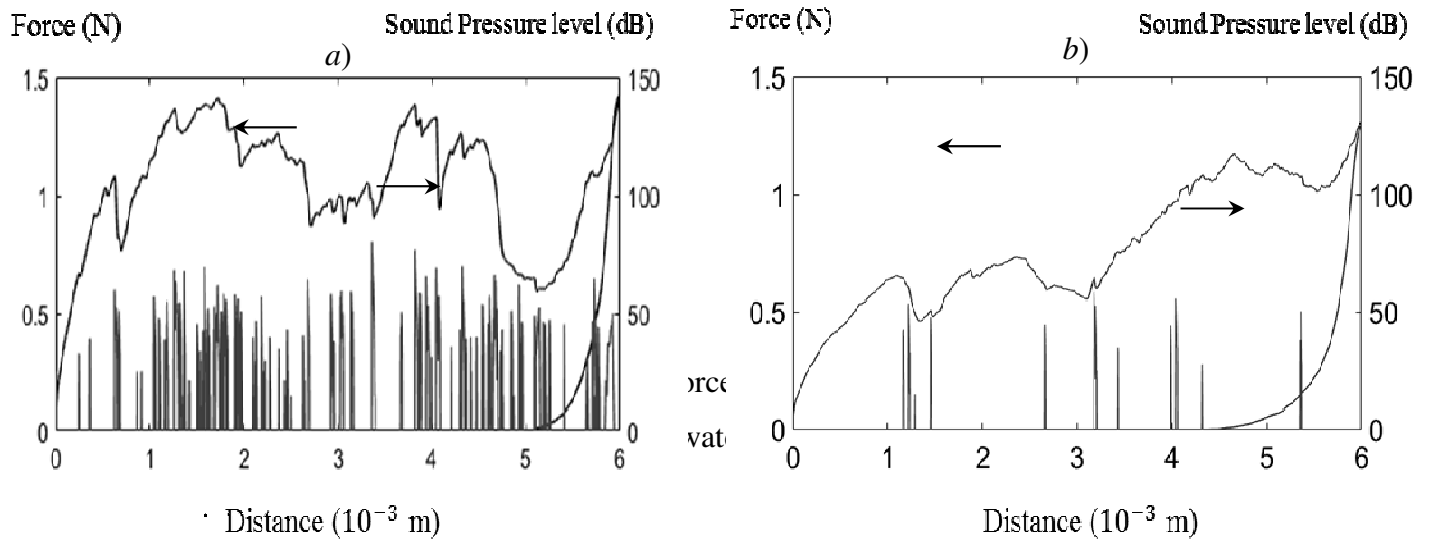


Figure 1.

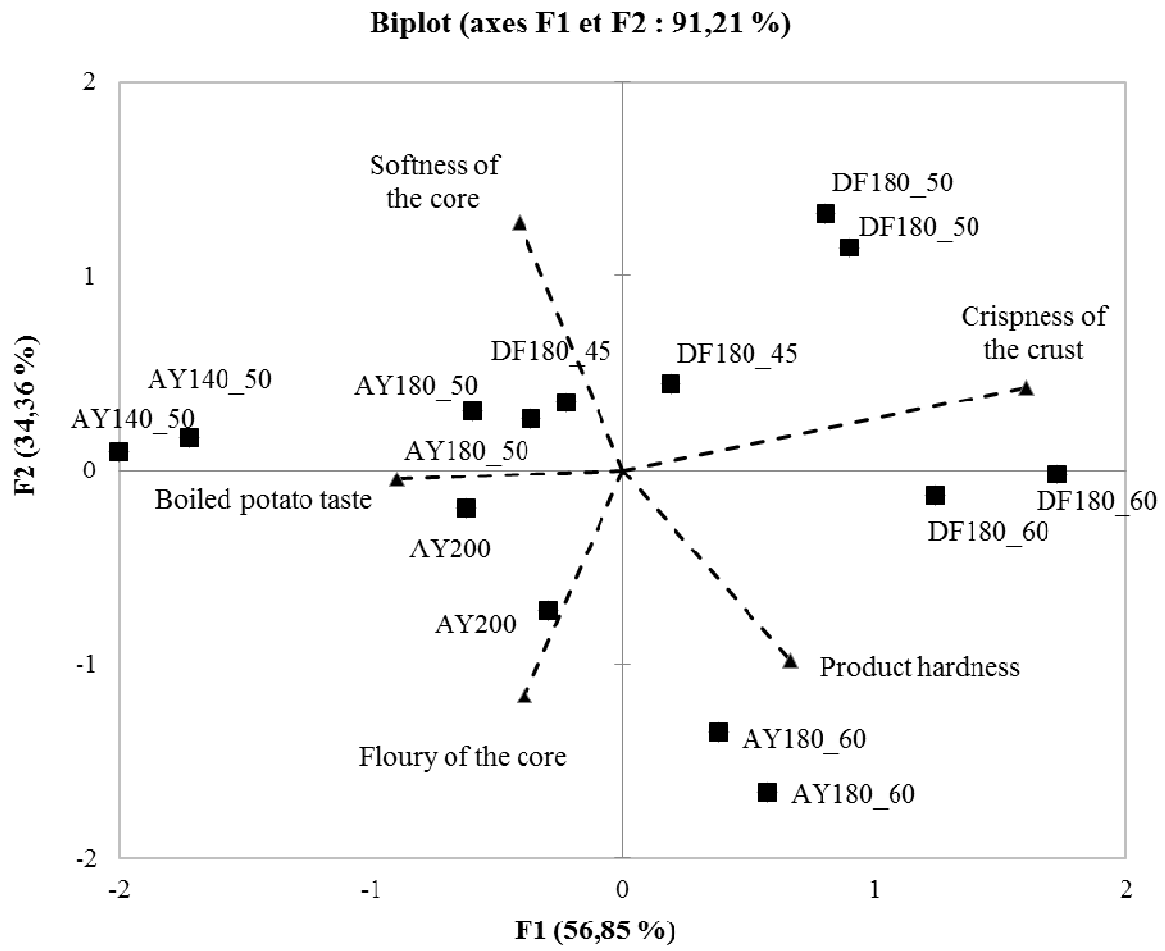


Figure 2.

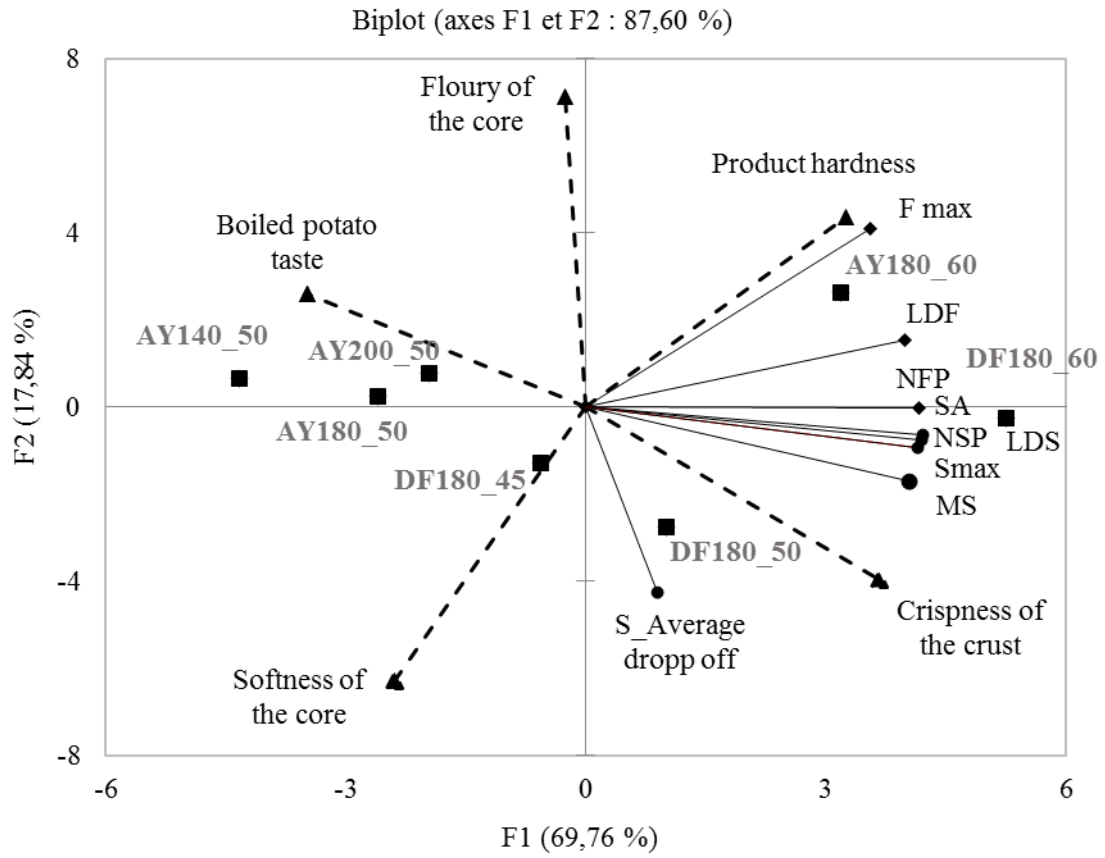


Figure 3.

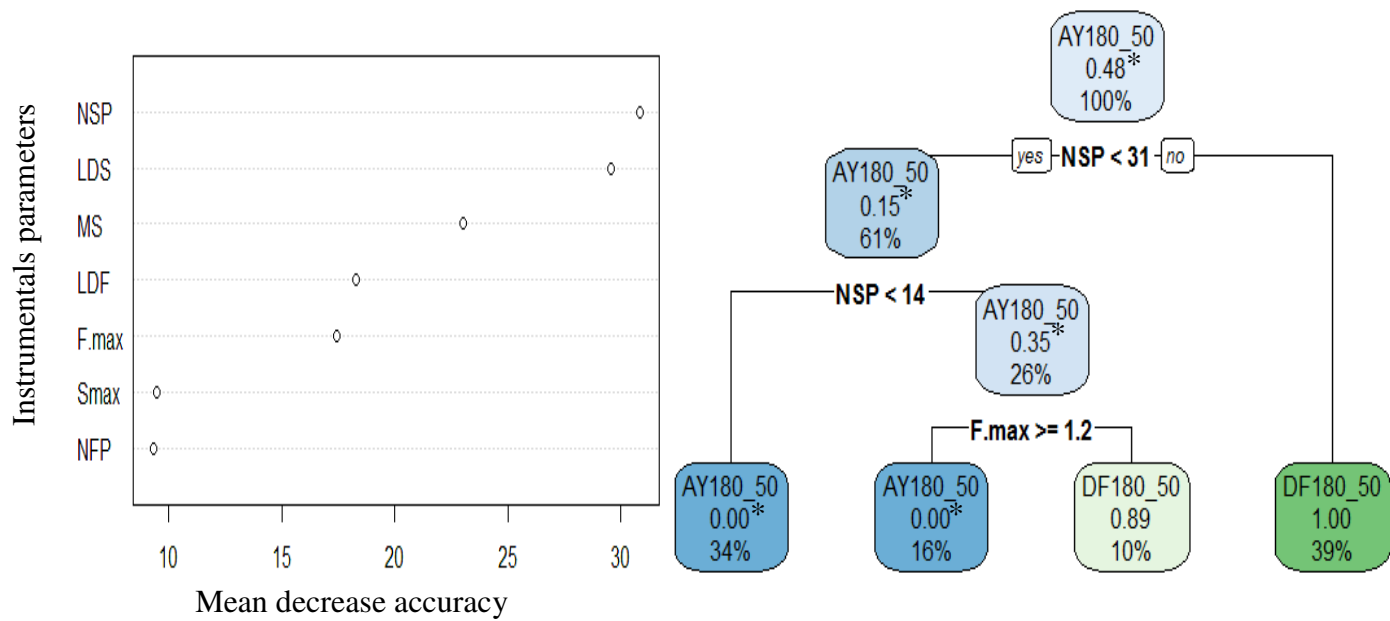


Figure 4:

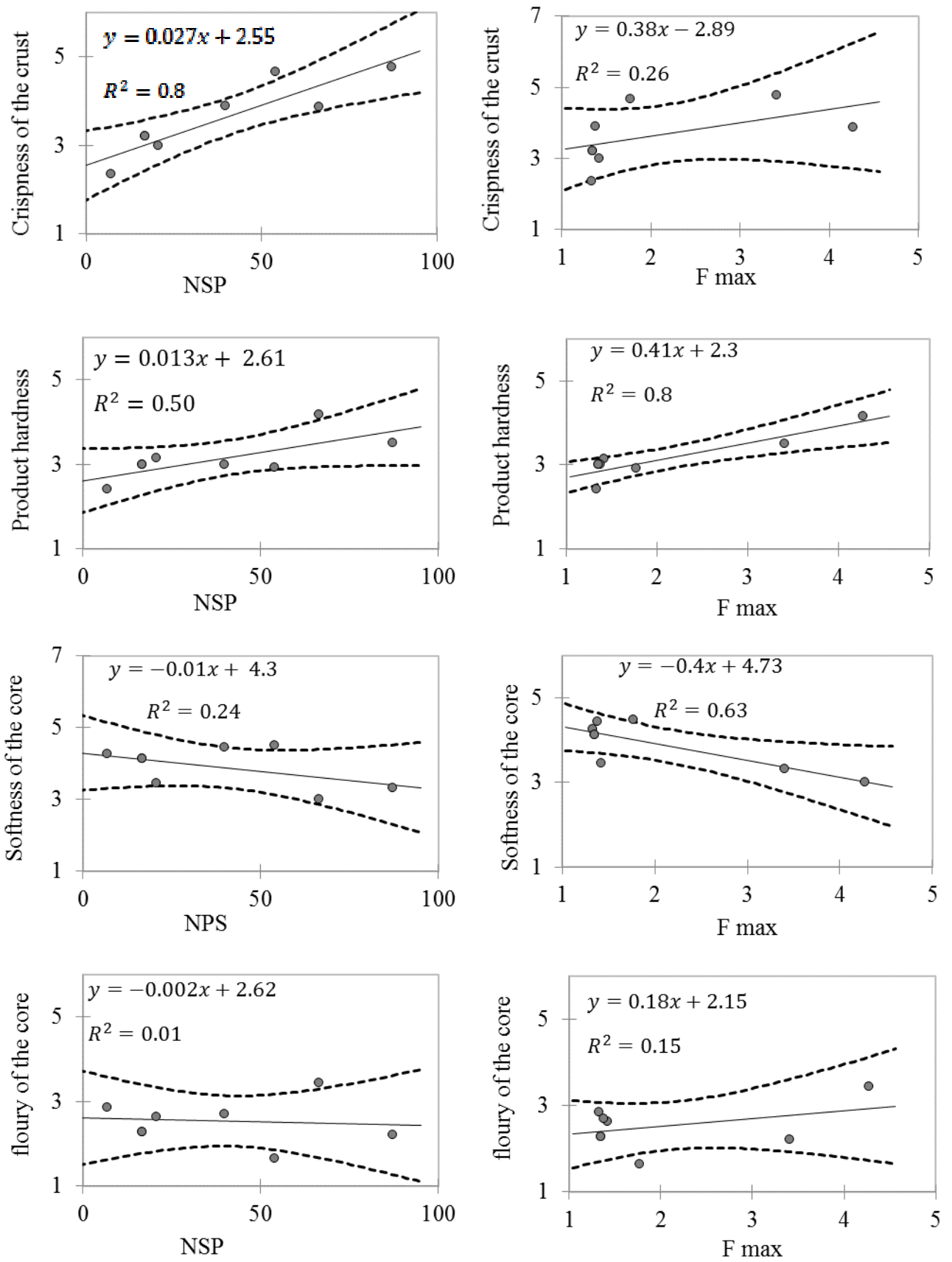


Figure 5.

