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Assessment of acoustic-mechanical measurements for 1 texture of French fries: Comparison of deep-fat frying 2 and air frying 3 4 5 Têko Gouvo^{*a*}, Christian Mestres^{*b*, *c*}, Isabelle Maraval^{*b*}, Bénédicte Fontez^{*d*}, Céline Hofleitner^{*a*}, Philippe Bohuon^{*e**} 6 7 8 ^a SEB, Ecully-Food Science; 112 Chemin du Moulin Carron, 69130 Écully 9 10 11 ^b CIRAD, UMR Oualisud, F-34398 Montpellier, France. 12 13 ^c Qualisud, Univ Montpellier, CIRAD, Montpellier SupAgro, Univ d'Avignon, Univ de 14 La Réunion, Montpellier, France. 15 16 ^d MISTEA, Montpellier SupAgro, INRA, Univ Montpellier, Montpellier, France, 17 ^e Qualisud, Montpellier SupAgro, CIRAD, Univ d'Avignon, Univ Montpellier, Univ 18 19 de La Réunion, Montpellier, France, 20 21 22 * Corresponding author: Philippe Bohuon, Montpellier SupAgro, UMR QualiSud, 1101 av. Agropolis, B.P. 5098, F-34093 Montpellier cedex 5, France. Tel. +33 467 87 23 24 40 81; Fax: +33 467 61 44 44. E-mail address: philippe.bohuon@supagro.fr

25 Abstract

26 The aim of this study was to develop an instrumental method for measuring the 27 texture of French fries and correlated it with sensory measurements. For seven samples 28 of French fries with different crispness levels, a cone penetrometer test was conducted 29 simultaneously with microphone recording of sound emissions. A descriptive sensory 30 analysis was also performed on these samples. The results showed that the number of sound peaks, the linear distance of sound peaks, the area under the sound-displacement 31 32 curve and the mean sound pressure were strongly positively correlated ($r \ge 0.80$; P-33 value < 0.02) with the crispness of the crust descriptor. The number of force peaks and 34 the linear distance of the force peaks were correlated with all the acoustic parameters. 35 These two mechanical parameters and the maximum force, were not correlated with 36 crispness of the crust (r = 0.50; P-value < 0.05) but strongly correlated with product hardness (r = 0.9; P-value < 0.01). However, the combination of the acoustic and 37 38 mechanical parameters appeared suitable for measuring the texture of French fries. An 39 analysis of the variable importance by random forest showed that the main parameters 40 for quantifying the texture differences were the number of sound peaks and the 41 maximum force. The use of this instrumental method and sensory analysis showed that 42 the deep-fat fried products were crispier than the air fried products with the same water 43 loss. 44 45

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54	Highlights (maximum 85 characters)
55	► Combination of acoustic and penetration tests are used to evaluate French fries
56	texture
57	► A high correlation exists between the sensory crispness and the acoustic
58	parameters
59	► The NSP and the Fmax makes it possible to clearly identify the crispness
60	► Deep-fat fried products are crispier than the air fried products with the same
61	water loss
62	Keywords
63	French fries; Hot air frying; Texture; Sensory analysis, Crispness; Acoustic properties.
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Abbreviations

Fmax	Maximum force
NFP	Number of force peaks
LDF	Linear distance of force peaks
F_Average	Average drop off of force peaks
Smax	Maximum of sound pressure
MS	Mean of sound pressure
AS	Area under sound displacement curve
NSP	Number of sound peaks
LDS	Linear distance of sound peaks
S_Average	Average dropp off of sound peaks
Т	Temperature (°C)
i.m	Initial mass

74 **1.** Introduction

75 French fries are a specific solid with a moist and soft core and a crispy outer dry 76 crust of approximately 1-2 mm (Bouchon & Aguilera, 2001; Pedreschi & Aguilera, 77 2002; Van Koerten, Schutyser, Somsen, & Boom, 2015). French fries are popular potato 78 products in many countries because of their structure and attractive texture. Texture is 79 one of the important quality aspects, and a crispy crust is a factor in the sensory 80 properties of French fries (Pedreschi & Aguilera, 2002; Salvador, Varela, Sanz, & 81 Fiszman, 2009). Crispness is one of the most important quality parameters in 82 consumers' choice of a fried product (L. M. Duizer, Campanella, & Barnes, 1998; 83 Luyten, Plijter, & Vliet, 2004; Salvador, Varela, Sanz, & Fiszman, 2009; Tunick et al., 84 2013). Many types of experiments have been conducted to determine crispness, but the 85 best measurements to assess crispness remain to be established (Gondek, Lewicki, & 86 Ranachowski, 2006; Luyten & Vliet, 2006; Castro-Prada, Luyten, Lichtendonk, Hamer, 87 & Vliet, 2007). This sensory attribute is often evaluated by sensory panel tests. 88 Unfortunately, sensory evaluations are expensive, unsuitable for routine testing and 89 generally provide a more qualitative than quantitative comparison (Zdunek, Cybulska, 90 Konopacka, & Rutkowski, 2011). Moreover, the results obtained from different sensory 91 panels are difficult to compare (Roudaut, Dacremont, Vallès Pàmies, Colas, & Le 92 Meste, 2002).

93 Several studies were carried out on the crispness of French fries using mechanical 94 tests (penetration, compression, bending). During a texture analysis, a force can be 95 exercised on a fried sample when a probe moves through it that imitates a first bite of 96 the product. Subsequently, the force-deformation curve is used to calculate the 97 quantitative parameters related to the crust fragility (Miranda & Aguilera, 2006; Van 98 Koerten, Schutyser, Somsen, & Boom, 2015). However, the results of the force-

99 deformation often do not show clearly a correlation with sensory crispness. 100 Nevertheless, Van Loon (2005) showed a correlation between the number of peaks in 101 the force-deformation and sensory perception of crispness of French fries. Instrumental 102 techniques present some advantages, especially in industrial environments in which 103 quick and easy-to-use methods are in great demand and are economically more 104 profitable (Saeleaw & Schleining, 2011). Other new texture measurement techniques, 105 such as acoustic measurements, have been used on crispy products other than French 106 fries, such as chips, wafer products, and have found high correlations with sensory 107 measurements (L. Duizer, 2001; Marzec, Cacak-Pietrzak, & Gondek, 2011; Saeleaw, 108 Dürrschmid, & Schleining, 2012; Carşanba, Duerrschmid, & Schleining, 2018). The 109 combination of acoustic and mechanical techniques has been shown to better describe 110 food texture than either of the two techniques alone (L. Piazza & Giovenzana, 2015; 111 Laura Piazza, Gigli, & Ballabio, 2007). The tests, mainly 3-point bending, penetration, 112 and compression methods, predicted the snack crunch (L. Duizer, 2001) and showed 113 good correlations between the acoustic-mechanical and sensory parameters. Other 114 studies have also shown that the sounds produced during food disintegration play an 115 important role in the perception of the texture of food materials (L. Duizer, 2001; 116 Luyten & Vliet, 2006). Sometimes these sounds describe the overall quality of a food 117 product better than any other sensory characteristic (A. marzec, G. cacak-pietrzak & E. 118 Gondek, 2011). The mechanical (penetration test) and acoustic evaluation of crispness 119 was also used to describe the texture of cookies (Chen, Karlsson, & Povey, 2005), 120 extruded bread (Marzec, Lewicki, & Ranachowski, 2007), toasted nuts (Salvador, 121 Varela, Sanz, & Fiszman, 2009) and apples (Zdunek, Cybulska, Konopacka, & 122 Rutkowski, 2011).

123 The aim of this study was to develop an instrumental method for measuring the 124 texture of French fries, and especially the crispness of the crust. A penetration test was 125 conducted simultaneously with microphone recording of sound emissions. A descriptive 126 sensory analysis was performed to evaluate the textural attributes, and the relationships 127 between the sensory parameters and the instrumental measurement parameters were 128 analysed. Finally, this approach was used to compare two products with contrasting 129 texture made using deep fat frying and air frying.

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131 **2.** Materials & Methods

132 **2.1.** Raw materials

133 The experiments were carried out with frozen French fries (Mc-Cain Tradition) 134 purchased at a local supermarket and stored in a cold room at -18 °C. The frozen 135 French fries were resized to 60 mm in length and 10 mm thick (10×10×60 mm) with a 136 specific cutter. Each experiment was conducted with 0.300 kg of sized French fries.

137 **2.2.** Frying equipment

Two main fryers were used: a commercial oil bath fryer (Filtra One FF162100
Seb) with a power of 1900 W, a chip capacity of 1.20 kg and an oil capacity of 2.10 L,
and hot-air frying equipment (Airfryer Philips XL HD9240/90, Avance Collection,
Amsterdam, The Netherlands) with a power of 2100 W.

142 **2.3.** Sample preparation

French fries with different crispness levels were obtained by adapting the frying equipment type, water loss and frying temperature.. Each experiment was carried out with 0.300 kg of sized French fries. Three French fries samples were fried at 180 °C with a conventional deep-fat fryer for final water losses of 60 %, 50 % and 45 %. Four French fries samples were prepared using the hot air fryer. Three of them were fried at 140 °C, 180 °C and 200 °C until the water loss reached 50 %. The fourth sample was 149 fried at 180 °C until a water loss of 60 %. The samples were coded according to their 150 frying conditions, as shown in Table 1. All French fries samples were analysed in under 151 5 min. The water loss was defined as the mass of water lost during frying divided by the 152 initial mass (i.m) of the sample before frying.

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2.4. Instrumental texture analysis

154 A penetration test was conducted with a conical probe with a 60° angle. 155 Mechanical (penetration test) and acoustic measurements were made using a texture 156 analyser (TA.XT.plus, Stable Micro Systems (SMS), Surrey, U.K) using a 5 kg sensor 157 connected to a microphone (Brüel Kjaer, Type 2671 Naerum, Denmark). This set was 158 placed in the Thermal Cabinet (TC/LN2 for the TA.XTplus Texture Analyser), which 159 was regulated at 50 °C. The microphone included an acoustic envelope detector (AED) 160 to avoid background noise. It was calibrated with a type 4231 acoustic calibrator (1 Hz, 161 Brüel Kjaer) at 94 and 114 dB sound pressure. The acoustic detector included a sound 162 amplification element that was set to level 2. The microphone position was 1.6 cm from the sample at an angle of 50°. Different test speed (0.2 mm.s⁻¹, 0.5 mm.s⁻¹, 1 mm.s⁻¹ 163 164 and 2 mm.s⁻¹) and deformation level (50 % and 80 %) were tried. The thermal cabinet 165 was turned off during the measurement due to the background noise of its fan. It was 166 used as a partition for the external environmental noise and for the sound emitted by the 167 sample. The conical probe was applied at a position of 20 mm from the extremity of the 168 French fry (1/3 of the length of the French fry). Each French fry was penetrated only 169 once. The measurements were carried out in triplicate with approximately fifteen French 170 fries per test.

171 The following parameters—maximum force (Fmax, N), number of force 172 peaks (NFP), linear force peak distance (LDF, Nm), maximum sound pressure level 173 (Smax, dB), mean of sound pressure (MS, dB), area under the sound displacement 174 curve (AS, dB m), number of sound peaks (NSP), linear distance of sound peaks (LDS, 175 dB m) and average drop-off of sound peaks (F Average, dB)—were evaluated with the 176 software Exponent (Stable Micro Systems) from the force-deformation curves and 177 acoustic displacement (Figure 1) in a range from 0 to 5 mm corresponding to 50% 178 deformation. The definitions of the instrumental parameters are described in detail 179 elsewhere (Varela, Salvador, & Fiszman, 2008; L. Piazza & Giovenzana, 2015; Kirmaci 180 & Singh, 2016). The sound pressure levels and force-deformation curves were recorded 181 with a detection threshold of 5 dB and 0.05 N, respectively. The same threshold values 182 were used for the detection of the number of sound peaks and the number of force 183 peaks.

- 184 **2.5.** Sensory analysis
- 185

2.5.1. Experimental conditions

186 A quantitative descriptive analysis (QDA) was used to evaluate the sensory 187 characteristics of the samples. The sensory profiles were performed in the sensory 188 analysis laboratory of the QualiSud UMR (CIRAD, Montpellier)). The room is 189 composed of 15 individual boxes including a small sink and an adaptable light. During 190 the tasting sessions, the room temperature and relative humidity were monitored and 191 averaged 22 \pm 4 °C and 29 \pm 6 %, respectively. Three or four French fries per 192 experimental conditions were presented in monadic form, 1 to 2 minutes after frying, in 193 petri dishes to keep the product warm. The panel consisted of 13 subjects (6 women and 194 7 men) aged 24 to 50 years, who were trained and qualified for sensory analysis 195 (repeatable, homogeneous).

196 **2.5.2.** *Descriptors*

Five descriptors of relevance were selected based on previous studies and considering the purposes of our study. The sensory descriptors studied were crispness of the crust, product hardness, softness of the core, floury of the core and boiled potato taste. The descriptors were evaluated on a continuous scale from the lowest intensity
(value 1) to the highest intensity (value 5). The definitions of and evaluation protocols
for the sensory descriptors are described in Table 2.

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2.5.3. Jury training

204 Before the tasting started, four training sessions, according to ISO 8586 (2012), 205 were carried out on four types of French fries. These were fried to present the average 206 and extreme intensities of each descriptor. The tasting panel was trained on the different 207 descriptors in the first two training sessions. The last two training sessions were 208 dedicated to assessing the panel's ability to use the descriptors. The scores assigned by 209 the judges were compared to those given by consensus, and judges were asked to 210 comply with the desired benchmark. The jury's training was validated by a statistical 211 analysis, analysing their repeatability. Non-repeatable judges were eliminated for the 212 remainder of the evaluation. Thirteen judges were validated.

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2.5.4. Tasting sessions

The seven French fries samples were coded and then submitted to the jury for analysis, giving a score ranging from 1 to 5 for each descriptor out of four tasting sessions. At each tasting session, three to four samples were presented in succession. The order of the samples was determined randomly. The tasting was then carried out in duplicate for each sample.

219 **2.6.** Statistical analysis

The statistical analysis of the results was carried out using XLSTAT version 2017 (ANOVA and PCA test) and R programs (decision tree test "rpart"). The ANOVA procedure at a significance level at 0.05 and the Tukey test were applied to assess significant differences between the investigated parameters. A correlation analysis (PCA) and a decision tree followed by a random forest were also conducted. An ensemble learner was built on decision trees, in which each decision tree was made with a bagging of observations and instrumental parameters. The mean decrease in accuracy caused by a parameter was determined during the out-of-bag error calculation phase from running the random forest 1000 times (number of trees = 1000, sample size = 63%, and no. of variables tried at each split = 2). The parameter importance estimated from the random forest was defined as the percentage of misclassifications.

- The results of the PCA analysis were presented as a two-dimensional graph: a graph that represents both variables and samples in two dimensions.
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234 **3.** Results and discussion

235 **3.1.** Sensory analysis

236 The ANOVA's results of the sensory analysis are summarized in Table 3. Seven 237 high-contrast texture samples were generated based on final water loss, frying method 238 and frying temperature. Five sensory descriptors were analysed. The floury of the core 239 was not significantly different for the seven samples. Its value ranged from 1.9 to 3.1. 240 This descriptor is not presented in Table 3. The crispness of the crust, product hardness, 241 softness of the core descriptors and boiled potato taste made it possible to classify the 242 seven samples into 4, 4, 2 and 3 groups, respectively. The variation coefficient of these 243 descriptors in the range from 4 and 10% was satisfactory. It was mainly the crispness of the crust (F-value = 44) and product hardness that differentiate the samples (F-244 245 value = 20). This is demonstrated in Figure 2, which presents the bi-plot PCA on 246 covariance, regarding the sensory descriptors data set for the seven French fries 247 samples. The average jury scores for the two tasting sessions are represented in Figure 2. The first two dimensions explain 91.2 % of the variability (56.8 % F1, 248 249 34.4 % F2). The crispness of the crust and boiled potato taste descriptors contribute 250 highly to the F1 axis respectively 62% and 20%. The product DF180_60 and 251 AY140 50 strongly drives the F1 axis. The axis F2 was more explained by the 252 descriptors softness of the core (39.5 %), floury of the core (32.7 %) and product 253 hardness (23.3 %). There was no correlation between the product hardness and the 254 crispness of the crust (r = 0.47; P-value < 0.05). Carsanba, Duerrschmid, & Schleining 255 (2018) also showed on wafer products that hardness and crispness were also slightly 256 correlated. In addition, the product hardness was strongly negatively correlated with the 257 softness of the core (r = -0.83; p-value < 0.02). The crispness of the crust was strongly 258 negatively correlated with only the boiled potato taste (r = -0.88; P-value < 0.01). The 259 PCA (Figure 2) shows that the seven French fries samples were repeatable quite varied 260 and well dispersed, thus explaining the different sensory descriptors. Afterwards, these 261 seven samples with contrasting textures were used to characterize the performance of 262 the instrumental measurements of texture.

263 **3.2.** Instrumental analysis: acoustics and force-deformation test

Four different test speeds were used $(0.2 \text{ mm.s}^{-1}, 0.5 \text{ mm.s}^{-1}, 1 \text{ mm.s}^{-1} \text{ and}$ 2 mm.s⁻¹), and two deformation levels (50 % and 80 %). The results showed that the use of a high test speed (2 mm.s⁻¹) dit not allow a significant difference between products, but a too low test speed (0.2 mm.s⁻¹) produces high significant differences but with a high variation coefficient (55 %). A moderate test speed of 0.5 mm.s⁻¹was used to make a successful compromise to minimize the variation coefficient. The deformation levels has no significant effect. The deformation level 50 % was used.

Figure 1 shows typical force-distance and acoustic amplitude-distance curves for two products: one very crispy and the other slightly crispy. In Figure 1 a), more acoustic and mechanical events were observed than in Figure 1 b). In Figure 1 b), when the force was at a maximum (1.2 N), no acoustic event was observed, whereas in Figure 1 a), when the force was at a maximum (1.4 N), there were more acoustic events. This showsthat the two products have different behaviours.

277 The maximum deformation forces did not exceed 5 N with a conical probe. This 278 value was in the same order of magnitude as reported by Kirmaci and Singh (2016) with 279 a penetration probe. The sound pressure level did not exceed 150 dB, which was in the 280 same order of magnitude as those determined by Carsanba, Duerrschmid, & Schleining 281 (2018) and Chen, Karlsson, & Povey (2005) on wafer products and biscuits 282 respectively. The sound pressure level was difficult to compare with the literature, as it 283 depended largely on the amplification level and the microphone location with regard to 284 the sample and on the product (Tunick et al., 2013). In most cases, the sound pressure 285 level ranged from 60 dB to 90 dB (Sanz, Primo-Martín, & van Vliet, 2007; Saeleaw et 286 al., 2012; Carsanba, Duerrschmid, & Schleining, 2018) for a crispy product.

287 These profiles (acoustic-distance and force-distance) made it possible to retrieve 288 the mechanical (penetration test) and acoustic parameters. All the experimental results 289 are gathered in Table 3 with an ANOVA (p-value < 0.05). Four mechanical (penetration 290 test) parameters were analysed, including the average drop-off of force peaks, which did 291 not allow any significant difference between the seven products. Thus, it will not be 292 discussed later. The number of force peaks (NFP) separated the samples into four 293 different groups. This parameter ranged from 13.3 to 1.9 among groups with a relative 294 uncertainty smaller than 25 %. The maximum force (Fmax) and linear distance of force 295 peaks (LDF) separated the samples in the same way. These parameters made it possible 296 to distinguish two product groups. For the LDF and Fmax parameters, the variation 297 ranges were 5.9 N m to 19.8 N m and 1.3 N to 4.3 N, respectively. The relative 298 uncertainty of these two parameters ranged from 4 to 20%. The number of force peaks 299 (NFP; F-value = 32.13) was more discriminating and provides different information 300 compared to Fmax (F-value = 30.71) and LDF (F-value = 19.3).

301 The analysis of the acoustic parameters showed that the number of sound 302 peaks (NSP) and the linear distance of sound peaks (LDS) followed the same rankings 303 by significantly separating the products into five different groups. The area under the 304 sound displacement curve (AS) and the mean of the sound pressure (MS) parameters 305 also grouped the samples in the same way by classifying them into four product groups. 306 For this reason, the area under the sound displacement curve (AS) was not presented in 307 Table 3. The relative uncertainty of these parameters ranged from 7 to 20 % for NSP (F-308 value = 60.7) and LDS (F-value = 58.3) and from 7 to 35 % for AS (F-value = 46.6) and 309 MS (F-value = 46.7). The maximum sound pressure (Smax) allowed the separation of 310 the products into four groups with both a low relative uncertainty (< 7 %) and a low 311 variation amplitude (75 to 50) when compared to the other acoustic parameters, such as NSP (87 to 7) and MS (10.5 to 0.5). By comparing the F-value of these acoustic 312 313 parameters, it can be observed that the Smax has a lower F-value (Smax, F-value = 23) 314 compared to the other parameters. The low F-value and low variation amplitude can 315 lead to a lack of efficiency of this parameter to detect significant differences when the 316 products to compare have a low texture difference.

The various acoustic parameters can be split into three groups (NSP/LDS, Smax and AS/MS), and the mechanical (penetration test) parameters into two groups (NFP and Fmax/LDF). The acoustic parameters separated the products into at least four groups with high F-value, while the mechanical parameters allowed their classification into two and four maximum groups with lower F-value than acoustic parameters. Therefore, the acoustic parameters are more sensitive than the penetration test parameters.

The analysis of the different confidence intervals and different F-values showed that mechanical responses were more repeatable (3 to 18 % relative uncertainty) but were less discriminating (low F-value) than acoustic responses (5 to 25 % relative 327 uncertainty). It is important to point out that the experimental variance was determined 328 with approximately forty-five values (French fries measured). This result shows that 329 this instrumental measurement was not as simple to carry out and required careful 330 implementation conditions to be reproducible.

331 **3.3.** Correlation between the results of instrumental and sensory analysis

332 Figure 3 shows a PCA on correlation, performed to illustrate the relation between 333 some mechanical (penetration test) and acoustic parameters and sensory descriptors of 334 French fries. The PCA showed that 87.60 % of the variability could be explained by the 335 first two main components: 69.76 % by the first component F1 and 17.84 % by the 336 second component F2. Instrumental parameters were projected as supplementary 337 variables and did not influence on the principal components of the analysis. The first 338 dimension (F1 axis) is particularly linked to the variables product hardness (29 %), boiled potato taste (29 %), crispiness of the crust (27 %) and softness of the core (15%). 339 340 The second axis is more related to the floury of the core (48 %) and the softness of the 341 core (20 %). This bi-plot illustrates that the products DF180_60 and DF180_50 were 342 associated with higher values of the acoustic parameters. These products were the 343 crispiest by sensory analysis. The AY180 60 product, which was considered harder and 344 moderately crispy, was associated with higher values of Fmax and product hardness. 345 The products AY40_50, AY180_50 and AY200_50 were characterized by lower values 346 of most of the acoustic parameters but were associated with higher values of boiled 347 potato taste. These products had the lowest crispness scores and were, therefore, 348 considered less crispy by the sensory analysis. Therefore, it can be concluded that an 349 increase in acoustic parameters reflects a high level of crispness. This is in line with 350 several previous works (Saeleaw & Schleining, 2011; Giacosa et al., 2016; Jakubczyk, 351 Gondek, & Tryzno, 2017; Çarşanba, Duerrschmid, & Schleining, 2018).

352 Some instrumental parameters were more or less correlated with each other, unlike 353 sensory parameters, which were distinct from each other (Figure 3). Most of the 354 acoustic parameters studied were positively correlated with each other, except for 355 the S_Average which was more closely related to the F2 axis. The acoustic parameters 356 NSP (r = 0.89; P-value < 0.01), LDS (r = 0.90; P-value < 0.01), Smax (r = 0.94; P-357 value < 0.01) and MS (r = 0.89; P-value < 0.01) were strongly positively correlated with 358 the crispness of the crust, with a high level of significance (Table 4). According to this, 359 a small number of acoustic events was considered as an indication of a low crispness of 360 the crust. This conclusion is in line with the work of Salvador, Varela, Sanz, & Fiszman 361 (2009), who obtained the same conclusion with potato chips. Smax, NSP and MS were 362 specifically used to explain the crispness and crunchiness of extruded snacks by 363 Saeleaw and Schleining (2011). In contrast, the sensory descriptor boiled potato taste 364 was negatively correlated to all these parameters (Figure 3). The crispier the products 365 were, the less the products taste like boiled potatoes.

366 The mechanical (penetration test) parameters were not significantly correlated with 367 crispness of the crust for P-value < 0.05 (LDF r = 0.70, P-value > 0.05; the 368 F max r = 0.5, P-value > 0.05), except for the NFP parameter (r = 0.84; P-369 value < 0.05). In contrast, F max was strongly correlated with the product 370 hardness (r = 0.9; P-value < 0.01). Obviously, the descriptor product hardness was not 371 only associated with the mechanical parameters. These results are in line with the work 372 carried out by Jakubczyk, Gondek, & Tryzno (2017) on co-extruded snacks. The 373 sensory descriptor softness of the core was negatively correlated to 374 F max (r = -0.79; P-value < 0.05) but not significant for the other instrumental 375 parameters. The harder the products were, the less soft the core was.

376 The relation between the parameters highly correlated with some evaluated sensory377 texture descriptors was established by analysing the linear regression

378 coefficients (Figure 5). The coefficient of determination (R^2) shows how the 379 instrumental parameters such as NSP and Fmax explain sensory descriptors (crispness 380 of the crust, product hardness, softness of the core or floury of the core) by a linear model. The parameters NSP ($R^2 = 0.80$) shows a high and positive regression coefficient 381 382 for the sensory crispness of the crust. This instrumental parameter allowed the 383 prediction of the sensory crispness of French fries correctly with high robustness. The 384 coefficient of determination of Fmax relative to hardness was high and reflects a strong correlation between hardness and F max ($R^2 = 0.80$). No parameter can significantly 385 predict the soft and floury of the core. This confirms that the two parameters (NSP and 386 387 Fmax) reflect the crispness and the product hardness. These results confirm that the two 388 methods provide different and complementary information. The mechanical parameters 389 had better explain the hardness of the product and the softness of the core, and the 390 acoustic parameters better explain the crispness of the crust. The combination of the 391 acoustic and mechanical (penetration test) methods seems appropriate to describe the 392 texture of French fries. Several other previous studies have reported the same 393 conclusion for other crispy food such as dutch crisbakes, wafers, crispy bakery products 394 (Mohamed, Jowitt, & Brennan, 1982; Laura Piazza, Gigli, & Ballabio, 2007; L. Piazza 395 & Giovenzana, 2015).

396 A random forest classification was carried out by comparing 45 deep-fat 397 fries (DF180_50) and 45 hot-air fries (AY180_50). The purpose was to detect the 398 importance of the variables in predicting the class of the French fries (between deep-fat 399 and hot-air). The products were made at the same frying temperature (180 °C) and with 400 the same water loss (50%). Figure 4 a) presents the classification tree relating the frying 401 process groups (deep-fat frying; air frying) to the instrumental parameters. The 402 parameter importance estimated from the random forest was defined as the percentage 403 of misclassifications. The more the accuracy of the random forest decreased due to the

404 exclusion (or permutation) of a single parameter, the more important that parameter was 405 deemed, and therefore, parameters with a large mean decrease in accuracy were more 406 important for the classification of the data. The acoustic parameters were more 407 important, especially the number of sound peaks (NSP) and the linear distance of sound 408 peaks (LDS), followed by the mean sound pressure (MS) and the area under the sound 409 displacement curve (AS). The parameters that have less weight were S_max and NFP. 410 Figure 4 b) shows a good discrimination of the products due to the parameters NSP and 411 Fmax and with an out-of-bag error of just 8.04 %. This confirms the relevance of 412 combining the acoustic parameters with NSP and the mechanical parameters with Fmax 413 with a performance error of 6.6 %. Other important instrumental parameters, such as 414 LDS, MS and AS, did not appear in the classification because they were highly 415 correlated with NSP and with each other. The combination of NSP and Fmax provides a 416 better classification of products. These results confirm also that a minimum hardness 417 (F max) was required to detect the crispness of French fries.

418 **3.4.** Impact of frying process on the texture

The analysis of Figure 1 showed that more acoustic and mechanical (penetration test) events were observed for the deep-fat fried products curve (Figure 1 a) than for the air-fried products (Figure 1 b). Teruel et al. (2015) also showed previously that the deep-fat fried fries are crispier than the air-fried fries.

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3 **3.4.1.** Effect of water loss

Three groups of French fries were generated according to their final water loss, ranging from 45 % to 60 %. An analysis of the sensory parameters did not make it possible to distinguish these three groups according to water loss. Only the Fmax, which reflects the hardness of the product, separated the samples into two groups. In the first group, all samples have a water loss of 60 %, and in the second group, the samples have

429 a final water loss of 45 % and 50 %. The more water was lost, the harder the product 430 became. For the other instrumental parameters, the effect of water loss was more 431 difficult to detect because of the combination of effects of process, temperature and 432 water loss. Indeed, it was possible to obtain the same water loss with different operating 433 conditions, and it was the rate of water transfer that was probably more important for 434 the texture of the product (Vitrac, Trystram, & Raoult-Wack, 2000; Bouchon & 435 Aguilera, 2001; Botero-Uribe, Fitzgerald, Gilbert, & Midgley, 2017). However, the 436 analysis of samples performed with deep-fat frying at 180 °C showed that an increase in 437 water loss increased the crispness of the crust and the product hardness. In contrast, the 438 softness of the core decreased with the water loss. In the instrumental parameters, there 439 was also an increase in mechanical and acoustic events as a function of water loss. For 440 comparing crispy products, it could be especially important to consider the water 441 content of the product (Seymour & Ann, 1988; Saeleaw, Dürrschmid, & Schleining, 442 2012)

443

3.4.2. Effect of air temperature

444 An analysis of the air-fried samples with the same water loss of 50 % showed that 445 an increase in frying temperature from 140 °C to 180 °C or 200 °C increased the values 446 of the crispness of the crust and product hardness. This is in line with several previous 447 works (Kita, Lisińska, & Gołubowska, 2007; van Koerten et al., 2015). The acoustic 448 parameter values also increased as the frying temperature increased. From 180 °C to 449 200 °C, the increase in the values of the various instrumental parameters analysed was 450 not significant. These results confirm the conclusions of van Koerten, Schutyser, 451 Somsen, & Boom (2015) that state that increased frying temperatures will improve the 452 crispy properties of the fries due to the formation of more and larger pores, but this 453 improvement only occurs until the temperature reaches a certain maximum, which was 454 between 180 and 195 °C. The sample (AY140_50) obtained by air frying at 140 °C has

the lowest values of crispness of the crust and product hardness but has the highest
value of softness at the core. The low air frying temperature (140 °C) was not sufficient
to develop a crispy crust, such as that developed at temperatures of 180 °C and 200 °C.
This difference is due to the low heat and mass transfer rates, which are responsible for
the development of the particular texture of fried products. (Loon, 2005; Kita, Lisińska,
& Gołubowska, 2007; Thussu & Datta, 2012; Zeb, 2019).

461

462

463 **4.** Conclusion

464 This study allowed the development of an instrumental method for measuring the 465 texture of French fries. The penetration test and acoustic signals provide different and 466 complementary information. Acoustic signals are very sensitive to the crispness of the 467 crust of French fries. Acoustic parameters, such as the number of sound peaks (NPS), 468 the linear distance of sound peaks (LDS), the maximum sound pressure (Smax), the 469 mean sound pressure (MS) and the area under the sound displacement curve (AS), are 470 highly correlated with the sensory crispness of the crust. The instrumental parameters 471 NSP, Smax and the maximum force (Fmax) are suitable for good characterization of the 472 texture of French fries, especially the crispness of the crust and the product hardness. 473 By using a combination of mechanical (penetration test) and acoustic approaches, it was 474 possible to better estimate the texture of French fries than by using one of the other 475 technique alone.

476 However, this method requires a large number of repetitions (about thirty French 477 fries) and requires careful implementation conditions to be reproducible. The 478 instrumental tests were able to evaluate, discriminate and reasonably predict the sensory 479 crispness of the crust of French fries, with an R^2 close to 0.8. In addition, the following 480 specific advantages make this approach suitable for industrial application.

481	The use of this instrumental method and sensory analysis showed that the deep-fat
482	fried products are crispier than the air fried products and that water loss has an effect on
483	the crispness and hardness of the fries. It is important to take into account the moisture
484	content when comparing the crispness or hardness of fried products.
485	
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Table 1: French fries samples condition obtained by deep fat frying (DF) or air frying (AY) at three different temperatures (for oil bath or air) and three different water loss level.

Sample's code	Frying equipment	T (°C)	Water loss (% i.m.)				
DF180_60	Deep-fat fryer	180	60				
DF180_50	Deep-fat fryer	180	50				
DF180_45	Deep-fat fryer	180	45				
AY180_60	Air fryer	180	60				
AY200_50	Air fryer	200	50				
AY180_50	Air fryer	180	50				
AY140_50	Air fryer	140	50				

Table 2: Definition and evaluation protocol of sensory descriptors

Sensory descriptors	Definition	Evaluation protocol	scoring scale
Crispness of the crust	Mechanical property related to the force required for the surface of the French fries to crumble or break during mastication	Put a French fry in the mouth and evaluate the force required to break the crust	1: Cardboardy 5: Crispy
Product hardness	Ability of the product to resist mechanical strain	Put a French fry in the mouth and evaluate the force required to break the whole French fry.	1: Soft 5: Hard
Softness of the core	Mechanical property related to the force required to obtain a deformation of the core of the French fries during mastication	Evaluate the force required to deform the product by compressing the core of the French fries between the teeth or between the tongue and the palate.	1: Hard 5: Soft
Floury of the core	Mechanical property related to the cohesion and presence of fine particles in the core of French fries during mastication	Put a French fry in the mouth and evaluate the presence of floury particles during mastication	1: Smooth 5: Floury
Boiled potato taste	Aroma of potato cooked in boiling water	Evaluate the intensity of the boiled potato aroma when tasting the French fries	1: Low 5: High

Table 3: Results of sensory analysis and instrumental tests for French fries samples obtained by deep fat frying (DF) or air frying (AY) at three different temperatures (140, 180 and 200 °C) and three different water loss level 45, 50 and 60 (% i.m).

Sample's code	Sensory descriptors				Mechanical test*			Acoustic test**					
	Crispness of the crust	Product hardness	Softness of the core	Boiled potato taste	NFP	LDF (10 ⁻³ N m)	Fmax (N)	NSP	LDS (10 ⁻³ dB m)	Smax (dB)	MS (dB)		
DF180_60	$4.9 \pm 0.2 a$	$3.5 \pm 0.3 ^{b}$	3.3 ± 0.3 ^b	1.9 ± 0.2 ^c	$13.3 \pm 3.5 a$	19.8 ± 3.7 ^a	$3.4 \pm 0.6 a$	87.1 ± 10.4	$a 6.9 \pm 1.3 a 7$	$5.3 \pm 3.5 a$	$10.4 \pm 2.3 a$		
DF180_50	4.7 ± 0.3^{a}	$2.9 \pm 0.3 ^{c}$	$4.5 \pm 0.2 a$	2.6 ± 0.3^{b}	$7.5 \pm 1.0 ^{c}$	9.2 ± 0.5^{b}	1.8 ± 0.2 ^b	54.0 ± 4.5	bc 4.4 ± 0.7 bc 6	$9.2 \pm 2.5 a$	5.6 ± 0.5 bc		
DF180_45	$3.9 \pm 0.3 ^{b}$	$3.0 \pm 0.2 ^{c}$	$4.5 \pm 0.2 a$	2.4 ± 0.5^{b}	$4.7 \pm 0.7 \ ^{cd}$	7.0 ± 0.3^{b}	1.4 ± 0.2 ^b	39.7 ± 3.1	c 3.3 ± 0.3 c 6	$7.4 \pm 3.8 ^{b}$	$3.8 \pm 0.3 ^{c}$		
AY180_60	$3.8 \pm 0.4 ^{b}$	$4.2 \pm 0.2 a$	3.0 ± 0.3 ^b	$2.7 \pm 0.5 ^{b}$	$9.9 \pm 1.3 \ ^{bc}$	15.0 ± 4.5 ^a	$4.3 \pm 0.6 a$	66.4 ± 9.3	b 5.3 ± 1.2 b 7	0.8 ± 3.3 ^b	6.5 ± 1.8 ^b		
AY200_50	$3.1 \pm 0.3 ^{c}$	$3.2 \pm 0.2 \ ^{bc}$	3.5 ± 0.3 ^b	2.6 ± 0.3^{b}	$2.9 \pm 0.7 ^{d}$	$6.3 \pm 0.4 ^{b}$	1.4 ± 0.2^{b}	20.7 ± 4.1	d 1.6 ± 0.2 d 5	9.0 ± 3.2 ^c	$1.6 \pm 0.5 ^{d}$		
AY180_50	$3.2 \pm 0.2 c$	$3.0 \pm 0.2 ^{c}$	$4.1 \pm 0.2 a$	2.8 ± 0.3 ^b	$2.9 \pm 0.7 ^{d}$	6.2 ± 1.2^{b}	1.3 ± 0.2^{b}	16.7 ± 3.5	d 1.3 ± 0.2 d 5	7.4 ± 2.6 ^{cd}	$1.2 \pm 0.3 ^{d}$		
AY140_50	2.4 ± 0.3^{d}	$2.4 \pm 0.3 d$	$4.3 \pm 0.2 a$	3.6 ± 0.2^{a}	$1.9 \pm 0.4 ^{d}$	5.9 ± 0.2^{b}	1.3 ± 0.3 ^b	6.9 ± 1.7	e^{e} 0.5 ± 0.1 e^{e} 5	$0.8 \pm 3.5 d$	0.5 ± 0.2^{d}		

Values are the mean \pm 95% confidence interval (n = 26 (2 tasting sessions \times 13 judges) for sensory analysis; $35 \le n \le 45$ for acoustical and mechanical analysis).

Means with the same superscript (a–e) within the same column do not differ significantly (Tukey test, *p*-value ≤ 0.05).

* NFP: number of force peaks; LDF: linear distance of force peaks; Fmax : maximum force

** NSP number of sound peaks; LDS: linear distance of sound peaks; Smax : maximum sound pressure level; MS: mean of sound pressure level

		Sensory descriptors					Mechanical parameters			Acoustic parameters				
	Variables	Crispness of the crust	Product hardness	Softness of the core	Floury of the core	boiled potato taste	NFP	LDF	F max	NSP	LDS	Smax	SAire	MS
Sensory descriptors	Crispness of the crust	1*												
	Product hardness	0.47	1*											
	Softness of the core	-0.12	-0.83*	1*										
	Floury of the core	-0.46	0.43	-0.51	1*									
	boiled potato taste	-0.88*	-0.54	0.35	0.43	1*								
cal ers	NFP	0.84*	0.70	-0.54	-0.09	-0.76	1*							
chani amet	LDF	0.70	0.72	-0.66	0.04	-0.68	0.97*	1*						
Mec	F max	0.50	0.89*	-0.79	0.39	-0.44	0.85*	0.89*	1*					
	NSP	0.89*	0.71	-0.49	-0.10	-0.81*	0.99*	0.93*	0.81*	1*				
ttic	LDS	0.90*	0.70	-0.47	-0.11	-0.81*	0.99*	0.92*	0.80*	1 *	1*			
Acous parame	Smax	0.94*	0.69	-0.37	-0.16	-0.87*	0.91*	0.81*	0.70	0.96*	0.97*	1*		
	SAire	0.89*	0.64	-0.46	-0.16	-0.81*	0.99*	0.95*	0.77	0.99*	0.99*	0.94*	1*	
	MS	0.89*	0.64	-0.46	-0.16	-0.81*	0.99*	0.95*	0.77	0.99*	0.99*	0.94*	1*	1*

Table 4: Matrix of correlation coefficients (*r*) between investigated variables.

The values of the correlation coefficients are different from 0 with a significance level alpha = 0.95

Values marked with an asterisk (*) correspond to correlation coefficients ≥ 0.8 indicating a high correlation.

NFP: number of force peaks; LDF: linear distance of force peaks; Fmax: maximum force

NSP number of sound peaks; LDS: linear distance of sound peaks; Smax: maximum sound pressure level; MS: mean of sound pressure level



Figure 1.



Figure 2.

Biplot (axes F1 et F2 : 91,21 %)



Figure 3.



Figure 4:



Figure 5.

