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## Modelling Spatial and Temporal Leaf Temperature Dynamics A focus on the leaf boundary layer

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**Highlights:** A 3D leaf temperature model is proposed to estimate dynamics of temperature gradients at leaf surface. The 3D leaf shape, the leaf physiology, and the microclimate are accounted for. Computational Fluid Dynamics was used to simulate realistic spatial evolution of the sensible heat flux at the leaf surface.

**Keywords:** 3D Leaf Model, Heat balance, Nusselt Number, Free Convection, Boundary Layer

### INTRODUCTION

Leaf temperature is an important factor involved in many biological processes such as leaf transpiration and photosynthesis (Gates 1968), leaf – pathogen interactions (Bernard et al. 2013) or insect development rates (Beck 1983). Within a plant canopy, leaves can exhibit a wide variety of temperature dynamics (frequency, amplitude, spatial gradients) related to the leaf position within the canopy (sunlit vs shaded leaf), the leaf shape and orientation (small vs large, downward vs upward), the leaf physiology (stomatal regulation), and the variability in microclimatic conditions (wind, light, air temperature and air relative humidity). Such variability in leaf temperature dynamics result from changes in heat energy exchanges between the leaf and its local environment. The underlying physics is well known and the temperature dynamics can be inferred by solving a heat balance equation where microclimate and leaf physiology are taken into account through radiation ( $R$ ), convection ( $C$ ), evapotranspiration ( $\lambda E$ ) and diffusion ( $G$ ) terms:  $R + C + \lambda E + G = 0$  (Monteith and Unsworth 1990). Among these terms, the convective term ( $C$ ) is definitively the more difficult to estimate because it describes the heat transfer process due to the leaf boundary layer.

Many leaf energy models have been developed so far and have been integrated in crop and plant canopy models (Sinoquet et al. 2001; Brisson et al. 2003) but they only simulate the dynamics of the spatially average leaf temperature. Our aim was to build up a flexible and fast 3D leaf temperature model to predict main trends of spatial temperature patterns dynamics at leaf surface. Both leaf geometry, leaf physiology and microclimate were accounted for (Fig. 1). Based on theoretical and Computational Fluid Dynamics (CFD) results, forced and free laminar boundary layers were implemented for the convective term. The free convective boundary layer implementation and the 3D model are presented and discussed.

### THE 3D LEAF TEMPERATURE MODEL

Among the different terms of the heat balance equation presented above, the diffusion term and the leaf thickness are neglected ( $G \approx 0$ ), based upon values of the leaf thickness ( $\sim 10^{-4}$  m) and the leaf thermal conductivity ( $0.4 \text{ W.m}^{-1}.\text{K}^{-1}$  (Vogel 1983)), and the time step used (from 30 minutes to one hour). Thus, the leaf volume is assumed to be zero and the surface is decomposed into  $n$  triangles.

On each triangle, the heat balance equation is solved following Monteith and Unsworth (1990):  $R + C + \lambda E = 0$ . The radiation heat flux is split into a direct and a diffuse component, and PAR and NIR wavebands are considered. The convective and evapotranspirative heat fluxes are modelled using classical relationships (Monteith and Unsworth 1990). The Jarvis model is used for the leaf stomatal conductance (Damour et al. 2010).

The entire leaf temperature model is written in Python. Numerical integrations and the iterative procedure used to solve the heat balance equation are based upon numpy and scipy libraries (Jones et al. 2001).

Both theoretical (plates) and real (3D scanned apple leaves) surfaces were used to assess the model and to perform temperature computations.

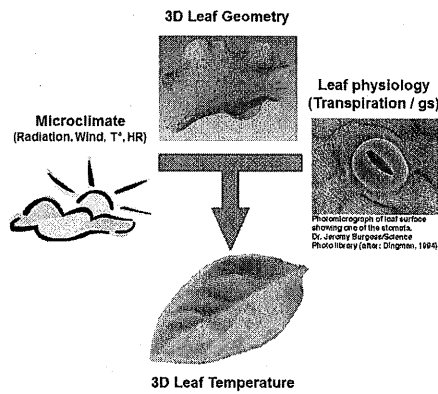


Fig. 1. Schematic view of the main features of the 3D leaf model

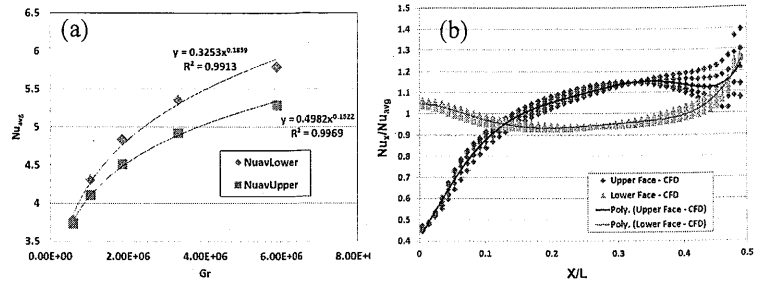


Fig. 2. Free convection – CFD results: (a) Average Nusselt number function of the buoyancy force intensity:  $Nu_{avg} = 1/L \int_L Nu_x dx$ , and (b) Local Nusselt number  $Nu_x/Nu_{avg}$  along the main axis for several Grashof numbers ( $X/L = 0$  corresponds to the plate center and  $X/L = 0.5$  to the edge of the plate).

## THE BOUNDARY LAYER

Loss of energy by the leaf boundary layer is highly dependent on the main force driving the flow (Schuepp 1993). For a leaf, two forces could induce a movement of the air at its surface: the inertial force due to the main outer flow (i.e. the wind speed  $U$ ), and the buoyancy force due to temperature gradient between the leaf surface ( $T_{leaf}$ ) and the air ( $T_{air}$ ). If the flow imposed by the external wind is weaker than the flow induced by the temperature difference between the leaf and the surrounding air, the convection is defined as "free". On the contrary if the boundary layer is driven by the external wind flow the convection is defined as "forced". The flow pattern and thus the heat exchange coefficient pattern dramatically change from a "free" to a "forced" convection. The convective heat transfer per unit of surface is defined by  $h(T_{leaf} - T_{air})$  where  $h$  is the heat transfer coefficient ( $W.m^{-2}.K^{-1}$ ). For convenience of scaling, the Nusselt number ( $Nu$ ) defined as  $Nu = \frac{h.L}{k}$ , where  $L$  is a characteristic length scale (m), and  $k$  is the thermal conductivity of air ( $W.m^{-1}.K^{-1}$ ), is used instead of  $h$  (Monteith and Unsworth 1990).

The intensity of free and forced convection can be estimated with the Grashof number (the ratio of buoyancy force to viscous force -  $Gr = \beta g L^3 (T_{leaf} - T_{air}) / \nu^2$ ) and the Reynolds number (the ratio of inertial force to viscous force -  $Re = UL/\nu$ ) (Monteith and Unsworth 1990) where  $\beta$  ( $K^{-1}$ ) is the thermal expansion coefficient of the air,  $g$  ( $m.s^{-2}$ ) is the acceleration of the gravity, and  $\nu$  ( $m^2.s^{-1}$ ) the kinematic viscosity of the air. Theoretical and experimental results have shown that the Nusselt numbers for free and forced convections are proportional to  $Gr^a$  and  $Re^b$  respectively (Schuepp 1993). The use of CFD (Comsol Multiphysics v4.3a) enables us to estimate the exponent coefficients  $a$  and  $b$  for a wide variety of driving force intensity and surface geometry.

Based on simple geometrical considerations (distance from the leaf leading edge according to the wind direction, distance from the leaf edge, main surface inclination angle) and estimates of Nusselt numbers from CFD, both kind of convection type were implemented in the 3D Leaf model.

## RESULTS AND DISCUSSION

Figure 2a shows the effect of Grashof number on average Nusselt numbers for a horizontal thin plate. For both faces the Nusselt number exhibits an exponential relationship with the Grashof number:  $Nu \sim m.Gr^a$  with  $a \approx 0.186$ ,  $m \approx 0.325$  for the lower face, and  $a \approx 0.152$ ,  $m \approx 0.498$  for the lower faces. These values are in agreement with the study of Wei et al. (2002) who performed numerical simulations of the natural convection heat transfer for an uniformly heated plate with metallic physical properties:  $a \approx 0.2$ ,  $m \approx 0.317$  and  $a \approx 0.16$ ,  $m \approx 0.675$  for the lower and upper faces respectively. Some heat transfer observations from uniformly heated metallic leaf models are available from early studies of Knoerr and Gay (1965) and Dixon and Grace (1983). They reported values of  $a$  between 0.1 and 0.2.

For several Grashof numbers i.e. free convection intensities, the ratio between the local Nusselt number  $Nu_x$  and the average Nusselt number  $Nu_{avg}$  (see figure 2a) along the main axis of the plate is plotted in figure 2b. For the range of Grashof numbers investigated, the ratio  $Nu_x/Nu_{avg}$  do not change with Gr except at the edge of the upper face. The Nusselt number presents different patterns between faces with a quasi flat curve at the lower face except at the edge, and with increasing values from the plate center to the edge for the

upper face. The ratio  $Nu_x/Nu_{avg}$  can be fitted with 5<sup>th</sup> and 6<sup>th</sup> order polynomial functions with R<sup>2</sup> coefficient up to 0.94 for lower and upper faces respectively.

The above CFD results show that some simple and robust relationships of heat transfer coefficients can be found for a free laminar convective boundary layer. Of course leaf boundary layers could exhibit local and sudden patterns for high inclination angle of the surface or when high wind velocity promotes the transition to turbulence of the leaf boundary layer, and the creation of large energetic structures in the trailing edge of the leaf. Such situations cannot be handled with the above relationships.

Above relationships of local and average heat transfer coefficients  $Nu_x(x/L)$  and  $Nu_{avg}(Gr)$  of free laminar convective boundary layer for both lower face and upper face were implemented in the 3D leaf model (figure 3a). Based upon such results and when all features of the 3D leaf model are used together, leaf temperature heterogeneity can be revealed (Figure 3b). In the future, a sensitivity analysis of the main parameters of the model and a model assessment based on IR infra-red camera measurements will be performed.

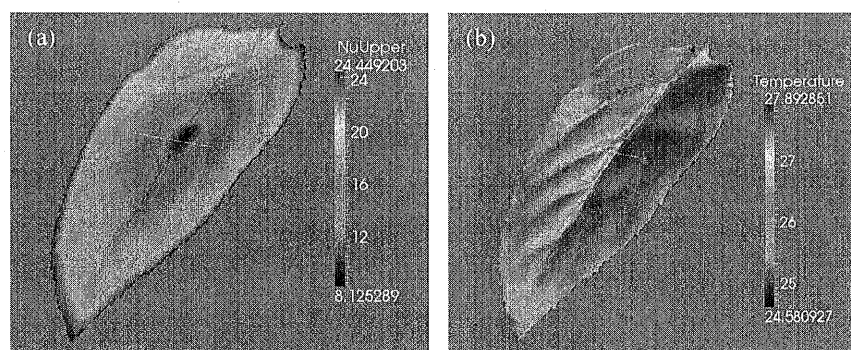


Fig. 3. Illustrations of (i) the Nusselt number implementation for a free convection for an horizontal 3D leaf model (a), and of (ii) a simulated temperature pattern according to given microclimate characteristics (b).

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