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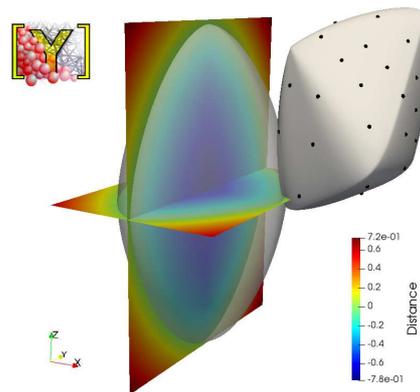


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## Graphical Abstract

**A Level Set-Discrete Element Method in YADE for numerical, micro-scale, geomechanics with refined grain shapes**

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# A Level Set-Discrete Element Method in YADE for numerical, micro-scale, geomechanics with refined grain shapes

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## Abstract

A C++-Python package is proposed for 3D mechanical simulations of granular geomaterials, seen as a collection of particles being in contact interaction one with another while showing complex grain shapes. Following the so-called Level Set-Discrete Element Method (LS-DEM), the simulation workflow stems from a discrete field for the signed distance function to every particle, with its zero-level set corresponding to a particle's surface. A Fast Marching Method is proposed to construct such a distance field for a wide class of surfaces. In connection with dedicated contact algorithms and Paraview visualization procedures, this shape description eventually extends the YADE platform for discrete simulations. Its versatility is illustrated on superquadric particles i.e. superellipsoids. On computational aspects, memory requirements possibly exceed one megabyte (MB) per particle when using a double numeric precision, and time costs, though also significant, appear to

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be lighter than the use of convex polyhedra and can be drastically reduced using a simple, OpenMP, parallel execution.

*Keywords:* Discrete Element Method (DEM), Level Set-DEM (LS-DEM), particle's shape, Fast Marching Method (FMM)

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## 1. Introduction

2 Geomaterials very often show a discrete nature which controls their solid-  
3 like strains or fluid-like strain rates while being under stress, e.g. granular  
4 soils. A proper description of that mechanical behavior is of interest to  
5 countless geo-engineering problems, e.g. the safe design of large rockfill dams  
6 (Deluzarche and Cambou, 2006), possibly rising in the order of hundreds  
7 of meters after piling up decimetric pieces of rock, or the forecast of snow  
8 mechanical stability and avalanches (Hagenmuller et al., 2015). Unlike the  
9 equivalent continuum descriptions classically used in engineering practice, nu-  
10 merical modelling approaches based on the Discrete Element Method (DEM,  
11 Cundall and Strack, 1979) duly respect this granular nature by describing the  
12 time evolution of a discrete set of particles, the so-called Discrete Elements  
13 (DE), in mechanical interaction. While DEM approaches often serve for  
14 qualitative studies in discrete geomechanics (e.g. Guo and Zhao, 2013; Duriez  
15 et al., 2018), they also are more and more often deployed for quantitative  
16 modelling (e.g. Aboul Hosn et al., 2017), possibly in a multiscale framework  
17 where a DEM description of a Representative Elementary Volume eventually  
18 substitutes constitutive relations in a FEM-like model (Miehe et al., 2010;  
19 Guo and Zhao, 2014).

20 On that quantitative point of view, the predictive abilities of DEM may  
21 appear as variable depending on the loading conditions (Aboul Hosn et al.,  
22 2017). As a matter of fact, they certainly often suffer from a spherical shape

23 assumption (adopted e.g. by Duriez et al., 2011; Guo and Zhao, 2013; Duriez  
24 et al., 2018; Aboul Hosn et al., 2017), since such spheres constitute a very  
25 strong simplification of material particles while particle’s shape has a known  
26 influence on the macroscopic behavior (e.g. Cho et al., 2006). Therefore, vari-  
27 ous DEM strategies towards a better shape description have been introduced,  
28 such as the use of rigid aggregates of spheres, so-called clumps, that should  
29 mimic real shapes (e.g. Garcia et al., 2009; Mede et al., 2018); or the di-  
30 rect consideration of polyhedra (e.g. Eliáš, 2014; Gladkyy and Kuna, 2017).  
31 Clumps offer the advantage to accommodate straightforward and compu-  
32 tationally cheap contact algorithms designed for spheres, but still present  
33 some unrealistic local roundness. On the other hand, polyhedra resort to  
34 more complex algorithms, which still remain restricted, most often, to con-  
35 vex surfaces (Dubois, 2011). One can also note the potential particles (PP)  
36 or potential blocks (PB) approaches by Houlsby (2009); Boon et al. (2012,  
37 2013), which both describe particles’ surfaces resorting to the zero-level of  
38 a so-called potential. Each scalar potential is given in a set of closed-form  
39 expressions with a variable number of shape parameters, leading to rounded  
40 (PP-case) or angular (PB-case) surfaces that are necessarily convex. Then,  
41 the so-called Level Set Discrete Element Method (LS-DEM) has been recently  
42 proposed by Kawamoto et al. (2016), in 3D, as another DEM extension to-  
43 wards realistic shapes. In LS-DEM, and with a limited similarity to PP and  
44 PB approaches, every DE’s surface is implicitly described as the zero-level  
45 set of the specific signed distance function to that surface. Contributing to  
46 its generality, no closed-form equation or convexity assumptions are required  
47 in LS-DEM since Level Set and Fast Marching Methods (Osher and Sethian,  
48 1988; Sethian, 1996, 1999) are available to construct distance fields for ar-  
49 bitrary, possibly concave, surfaces and a wide class of scientific applications

50 (e.g. Yang et al., 2019). Kawamoto et al. (2016, 2018) actually illustrated  
51 the capabilities of the LS-DEM to describe real soil grains, shapes being ac-  
52 quired through X-ray computed tomography, as well as its promising features  
53 to reproduce observed behaviors both qualitatively and quantitatively.

54 The present contribution then proposes an independent and original im-  
55 plementation of LS-DEM into the existing YADE open-source platform (Šmilauer  
56 et al., 2015), which is often used for geo-mechanical simulations (e.g. Duriez  
57 et al., 2011; Boon et al., 2013; Duriez et al., 2018; Aboul Hosn et al., 2017;  
58 Pirnia et al., 2019). Example usages are furthermore provided for complex,  
59 superquadric shapes, alongside discussing computational costs in comparison  
60 with the polyhedral shape description.

61 Section 2 first recalls Level Set and Fast Marching Methods serving to  
62 establish distance fields for arbitrary surfaces. Then, Section 3 describes how  
63 LS-DEM uses the particles' distance fields for DEM simulations of granular  
64 soils, usually following here the initial guidelines of Kawamoto et al. (2016) or  
65 Duriez and Bonelli (2021). An original LS-DEM code is proposed accordingly  
66 and summarized in Section 4. Section 5 and 6 present a direct application  
67 to non-spherical, superquadric, shapes with illustrative simulations and a  
68 computational comparison with the use of convex polyhedra.

## 69 **2. Level Set and Fast Marching methods**

### 70 *2.1. Level set formalism*

71 Level set approaches (Osher and Sethian, 1988; Sethian, 1999) see in-  
72 terfaces  $\mathcal{S}(t)$  as the zero-level set of a function  $\phi^t(\vec{x}, t)$  being defined from  
73  $\mathbb{R}^d \times \mathbb{R}$  into  $\mathbb{R}$ , with  $\mathbb{R}^d$  covering the whole space of a  $d$  dimensionnality.  
74 Evolving contours (resp. surfaces) can then be described for  $d = 2$  (resp.  
75  $d = 3$ ). While the interfaces evolve, propagating with a normal velocity

76  $\vec{v} = F(\vec{x}, t) \vec{n}$  (where  $\vec{n}$  stands for the outwards normal), all level sets evolve  
77 with an extended velocity parallel to the gradient of the level set function  
78  $\phi^t(\vec{x}, t)$ . Since  $\phi^t(\vec{x}, t)$  is constant along  $\mathcal{S}(t)$  (equal to 0  $\forall t$ ), the nullity of  
79 the material derivative along the interface front leads to the following level  
80 set equation:

$$\frac{\partial \phi^t}{\partial t} + F \|\vec{\nabla} \phi^t\| = 0 \quad (1)$$

81 Eq. (1) conforms the formalism of Hamilton-Jacobi partial derivative  
82 equations (Osher and Sethian, 1988), with the Hamiltonian  $H^t$ , as a function  
83 of the spatial derivative(s) of  $\phi^t$ , being equal to:

$$H^t(\phi_x^t) = F |\phi_x^t| \quad \text{for } d = 1 \quad (2)$$

$$H^t(\phi_x^t, \phi_y^t) = F \sqrt{\phi_x^{t2} + \phi_y^{t2}} \quad \text{for } d = 2 \quad (3)$$

$$H^t(\phi_x^t, \phi_y^t, \phi_z^t) = F \sqrt{\phi_x^{t2} + \phi_y^{t2} + \phi_z^{t2}} \quad \text{for } d = 3 \quad (4)$$

84 where  $f_x, f_y, f_z$  stand for the spatial derivatives of any scalar function  $f$  with  
85 respect to  $x, y, z$ .

86 The signed (shortest) distance to  $\mathcal{S}(t)$  is a typical choice for the function  
87  $\phi^t$ , with the convention of a negative, resp. positive, distance when being  
88 inside, resp. outside, of  $\mathcal{S}(t)$ . Doing so, and for a constant and uniform speed  
89  $F(\vec{x}, t) = F$ , one can relate  $\phi^t$  to  $T(\vec{x})$ , the arrival time of  $\mathcal{S}$  at  $\vec{x}$ :

$$\phi^t(\vec{x}, t) = F (T(\vec{x}) - t) \quad (5)$$

90 Inserting Eq. (5) into the level set equation (1), one easily re-obtains the  
91 so-called Eikonal equation:

$$F \|\vec{\nabla} T\| = 1 \quad (6)$$

92 With respect to the use of  $\phi^t$  and the level set Eq. (1), the consideration  
93 of  $T$  and the Eikonal Eq. (6) forms another description of evolving interfaces,  
94 adapted to the case of a constant and uniform sign for the normal velocity.

95 Doing so, the current interface  $\mathcal{S}(t)$  is the  $t$ -level set of  $T$  and no time variable  
 96 enters the partial differential equation (6). That stationary perspective can  
 97 be finally complemented by the consideration of  $\phi(\vec{x})$ , the distance to  $\mathcal{S}(t =$   
 98  $0)$ :

$$\phi(\vec{x}) = \phi^t(\vec{x}, 0) = F T(\vec{x}) \quad (7)$$

99 with the following form for the Eikonal equation:

$$\|\vec{\nabla}\phi\| = 1 \Leftrightarrow H(\phi_x, \dots) = 1 \quad (8)$$

100 Similar to Eqs. (1)-(4), Eq. (8) can be cast in the form of a Hamiltonian

101  $H(\phi_x, \dots) = 1$  with:

$$H(\phi_x) = |\phi_x| \quad \text{for } d = 1 \quad (9)$$

$$H(\phi_x, \phi_y) = \sqrt{\phi_x^2 + \phi_y^2} \quad \text{for } d = 2 \quad (10)$$

$$H(\phi_x, \phi_y, \phi_z) = \sqrt{\phi_x^2 + \phi_y^2 + \phi_z^2} \quad \text{for } d = 3 \quad (11)$$

## 102 2.2. A Fast Marching Method for the stationary perspective

103 Looking for the distance field  $\phi$  to a given, constant, surface  $\mathcal{S}$ , the Eikonal  
 104 equation (8) can be efficiently solved using a so-called Fast Marching Method  
 105 (FMM, Sethian, 1996, 1999). Space being discretized on a grid, the Eikonal  
 106 equation makes the  $\phi$ -value at some gridpoint  $\vec{x}_i$  being directly dependent  
 107 upon surrounding  $\phi$ -values at adjacent gridpoints, as can be seen from finite  
 108 difference expressions for the spatial derivatives in Eqs. (9) to (11). Account-  
 109 ing for the monotonous nature of  $\phi$ , which strictly increases (in absolute  
 110 value) when  $\vec{x}$  goes away of  $\mathcal{S}$ , the FMM eventually gives the full discrete  
 111 field  $\phi(\vec{x}_i)$  starting from an initial set of gridpoints being along, or close to,  
 112 the surface and serving as boundary conditions. In more details, the FMM  
 113 recursively applies Eq. (8), in the form of Eqs. (9) or (10) or (11) depending  
 114 on gradient's dimensionality, and adopting gradient expressions decentred

115 to low and known  $\phi$ -values. Recursive applications actually go in a down-  
 116 wind direction away from the surface, until the whole spatial grid has been  
 117 handled. The key point of the FMM is to go through the grid points in the  
 118 right order, following at each step the minimal value of distance.

119 The FMM for instance directly applies to any surface  $\mathcal{S}$  showing a scalar  
 120 inside/outside function  $f(\vec{x})$ , being positive (resp. negative) for  $\vec{x}$  located  
 121 outside (resp. inside) the surface and null along the surface. In such a case,  
 122 boundary conditions gridpoints are easily identified as all gridpoints being  
 123 outside of the surface and having a grid neighbor inside and they can be  
 124 assigned the following  $\phi$ -value:

$$\phi(\vec{x}) = \frac{f(\vec{x})}{\|\vec{\nabla}f(\vec{x})\|} \text{ for } \vec{x} \text{ close to } \mathcal{S} \quad (12)$$

125 By construction, Eq. (12) is a first order approximation to  $\phi$ , obviously obey-  
 126 ing  $\phi = 0$  along  $\mathcal{S}$  and also verifying the Eikonal equation (8) close to  $\mathcal{S}$ ,  
 127 provided that  $\vec{\nabla}(1/\|\vec{\nabla}f\|)$  is finite. This constitutes the initialization of the  
 128 distance function on the grid points close to the interface, before applying  
 129 the recursive operations of the FMM.

130 Figure 1 illustrates the distance output of such a FMM procedure, herein  
 131 implemented in a `DistFMM` C++ class presented in Section 4.1, when applied  
 132 to the following “flake-like” inside/outside function:

$$f(\vec{x}) = r - [R + \Delta R \sin(5\theta) \sin(4\varphi)] \quad (13)$$

133 In Eq. (13),  $(r, \theta, \varphi)$  refer to spherical coordinates with  $\theta \in [0; \pi]$  measured  
 134 from  $\vec{z}$  axis and  $\varphi \in [0; 2\pi]$  measured in  $(\vec{x}, \vec{y})$  plane.

### 135 3. LS-DEM formulation

136 For any DEM mechanical simulation to progress in time, it is first nec-  
 137 essary to describe the shapes of the bodies, i.e. DEs, and detect their pos-

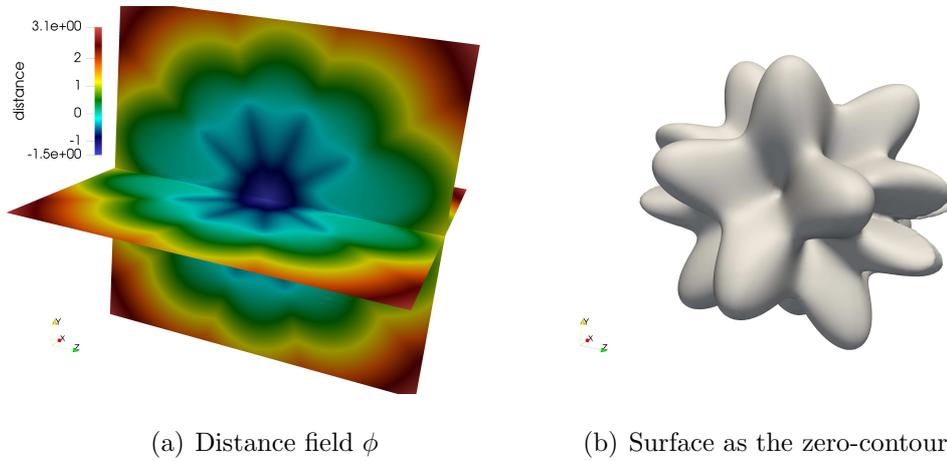


Figure 1: Level Set description of a flake-like surface defined by Eq. (13), with  $(R; \Delta R) = (3; 1.5)$ , after executing a FMM on a 0.1-spaced isotropic grid

138 sible contact interactions with neighbors. Then, contact-scale constitutive  
 139 relationships express forces and torques so that rigid motion equations can  
 140 finally be integrated. The following sections detail these three steps.

### 141 3.1. LS-DEM shape description

142 Following Kawamoto et al. (2016, 2018), a discrete signed distance field  
 143 on a body-centered regular grid, possibly obtained from the previous FMM,  
 144 is the first LS-DEM ingredient. That (grid ; distance field) pair is in-  
 145 dependently defined for every DE in a local coordinate system and first  
 146 serves for defining the DE inertial quantities (mass  $m$  and inertia matrix  
 147  $\mathbf{I} = I_{\alpha\beta}, \alpha, \beta \in \{x, y, z\}$ ) summing contributions from grid voxels  $v$  making

148 up the body's volume  $V$  as per the following discrete-form equations:

$$m = \rho \sum_{v \in V} V_v = \rho N_{vox} V_v \quad (14)$$

$$\vec{x} = \frac{1}{N_{vox}} \sum_{v \in V} \vec{x}_v \quad (15)$$

$$I_{xx} = \rho \sum_{v \in V} [(y_v - y)^2 + (z_v - z)^2] V_v \quad (16)$$

$$I_{yy} = \rho \sum_{v \in V} [(x_v - x)^2 + (z_v - z)^2] V_v \quad (17)$$

$$I_{zz} = \rho \sum_{v \in V} [(x_v - x)^2 + (y_v - y)^2] V_v \quad (18)$$

$$I_{xy} = -\rho \sum_{v \in V} (x_v - x) \times (y_v - y) V_v \quad (19)$$

$$I_{xz} = -\rho \sum_{v \in V} (x_v - x) \times (z_v - z) V_v \quad (20)$$

$$I_{yz} = -\rho \sum_{v \in V} (y_v - y) \times (z_v - z) V_v \quad (21)$$

149 In the above equations,  $\rho$  is the material mass density,  $\vec{x}_v = (x_v, y_v, z_v)$   
 150 the middle point of a voxel and  $\vec{x} = (x, y, z)$  the body's center of mass. Eqs.  
 151 (15),(19)-(21) serve for verification purposes since the body-attached local  
 152 frame is expected to be inertial and  $\vec{x}, I_{xy}, I_{xz}, I_{yz}$  to be nil. By a simple  
 153 convention, a grid voxel  $v$  of volume  $V_v$  is herein said to be part of the  
 154 body's volume  $V$  when its lowest corner is inside the surface, showing a zero  
 155 or negative distance value. While smoother choices have been proposed by  
 156 Kawamoto et al. (2016, 2018), it will be verified in Section 5.2 that the present  
 157 choice does not inhibit precision for grids being fine enough, i.e. showing a  
 158 spacing  $g_{grid}$  at least ten times smaller than a grain's characteristic size  $l_{grain}$ .

159 For the purpose of LS-DEM contact algorithms that will be described in  
 160 Section 3.2 below, a second LS-DEM ingredient adds to the distance field, in  
 161 the form of a set of  $N_n$  boundary nodes  $\{N_i, i \in [0; N_n - 1]\}$  discretizing each  
 162 body's surface  $\mathcal{S}$ . Generally speaking, boundary nodes should count in the

163 order of thousands and their positions are defined at the intersection of  $\mathcal{S}$  i.e.  
 164  $\phi(\vec{x}) = 0$  and  $N_n$  half-lines i.e. rays  $\lambda\vec{v}$ , with  $\vec{v}$  a direction and  $\lambda$  a positive  
 165 abscissa, that stem from the center of mass. Due to the adopted tri-linear  
 166 interpolation of the discrete distance field within the grid extents,  $\phi(\vec{x} = \lambda\vec{v})$   
 167 is a cubic polynomial in  $\lambda$  whose coefficients depend upon grid distance val-  
 168 ues and ray tracing boundary nodes corresponds to solve its positive roots  
 169 (see e.g. Lin and Ching, 1996). Since rays should provide an appropriate dis-  
 170 cretization of spherical angles  $(\theta, \varphi)$ , the corresponding directions  $(\theta, \varphi)$  are  
 171 chosen to follow a spiral path instead of a simple rectangular discretization of  
 172  $[0; \pi] \times [0; 2\pi]$  in order to avoid a possible (shape-dependent) concentration  
 173 of nodes at the poles  $\theta = 0[\pi]$ . More details about the spiral path or the  
 174 choice of boundary nodes number are given by Duriez and Bonelli (2021) and  
 175 in the next sections.

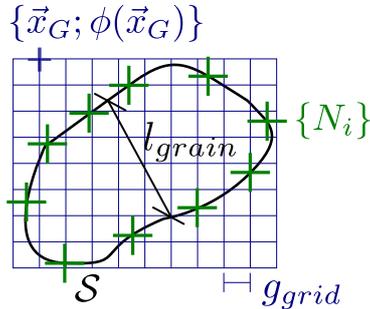


Figure 2: Shape description in LS-DEM: a regular grid  $\{\vec{x}_G\}$  carrying the distance field  $\phi$ , together with boundary nodes  $\{N_i\}$  (2D view for clarity)

176 Figure 2 illustrates these LS-DEM ingredients which all refer to a constant  
 177 shape-related (inertial) local frame and never need to be updated. Assum-  
 178 ing rigid particles, the subsequent contact algorithm easily switches between  
 179 global and local frames during simulations.

180 *3.2. Contact law*

181 From the distance fields and the set of boundary nodes, contact detec-  
 182 tion between two bodies 1 and 2 relies on a master-slave algorithm whereby  
 183 nodes  $N_i^1$  of body 1 are tested in the distance field  $\phi_2$  of body 2 (see also  
 184 Figure 9). In order to increase precision, the body 1 is chosen as the small-  
 185 est one in volume, which enables one to explore distance fields with the  
 186 greatest surface density in nodes. Contact is detected as soon as one node  
 187  $N_i^1$  verifies  $\phi_2(N_i^1) \leq 0$ . LS-DEM belongs to the wide class of “soft” DEM  
 188 whereby small overlaps,  $\phi_2(N_i^1) < 0$ , are possible: these overlaps would in  
 189 reality materialize through slight changes in shape which are neglected in soft  
 190 DEM approaches. After identifying the set of contacting boundary nodes, a  
 191 unique contact point is herein chosen from the node  $N_c$  showing the greatest  
 192 interpenetration depth  $u_n$ , which also gives the contact normal as the local  
 193 gradient of  $\phi_1$ :

$$u_n = -\min(\phi_2(\overrightarrow{ON}_i), \overrightarrow{ON}_i \in \mathcal{S}_1) = -\phi_2(\overrightarrow{ON}_c) \geq 0 \quad (22)$$

$$\vec{n} = \vec{\nabla}\phi_1(\overrightarrow{ON}_c) \quad (23)$$

194 That final consideration of a unique contacting point, also adopted by  
 195 Li et al. (2019), currently restricts the proposed LS-DEM implementation to  
 196 convex shapes. For a pair of contacting bodies with concave shapes, multi-  
 197 ple contact points would occur but these could be easily detected with the  
 198 same master-slave algorithm. As such, Kawamoto et al. (2016, 2018) also  
 199 addressed concave shapes by defining a mechanical interaction at each con-  
 200 tacting boundary node. While being more general, this choice nevertheless  
 201 poses the risk to make the macroscopic behavior, e.g. the bulk stiffness, to di-  
 202 rectly depend upon the chosen number of boundary nodes in case a physically  
 203 unique contact area would involve more than one boundary node.

204 A classical contact law for cohesionless materials finally expresses the  
 205 interaction force after decomposing the latter in a normal, along  $\vec{n}$ , and a  
 206 tangential component. A repulsive normal force  $\vec{F}_n$  first arises due to the  
 207 interpenetration depth  $u_n$ , as per a linear elastic model with a  $k_n$  stiffness:

$$\vec{F}_n = k_n u_n \vec{n} \quad (24)$$

208 Along the tangential direction, a linear elastic-plastic relationship governs  
 209 the shear force variations. Denoting  $k_t$  the shear stiffness and  $\mu$  the friction  
 210 coefficient, the following Eqs. (25)-(26) describe the variations of the shear  
 211 force  $\vec{F}_t$ , starting from  $\vec{0}$ :

$$d\vec{F}_t = d \left( \|\vec{F}_t\| \frac{\vec{F}_t}{\|\vec{F}_t\|} \right) = \|\vec{F}_t\| d \left( \frac{\vec{F}_t}{\|\vec{F}_t\|} \right) + d(\|\vec{F}_t\|) \frac{\vec{F}_t}{\|\vec{F}_t\|} \quad (25)$$

$$d(\|\vec{F}_t\|) \frac{\vec{F}_t}{\|\vec{F}_t\|} = k_t d\vec{u}_t \quad \text{enforcing } \|\vec{F}_t\| \leq \mu \|\vec{F}_n\| \quad (26)$$

212 while updates in the shear force direction,  $\vec{F}_t/\|\vec{F}_t\|$ , are applied in order to  
 213 follow changes in the tangent plane's orientation, e.g. a change in contact  
 214 normal (Šmilauer et al., 2015).

### 215 3.3. Motion integration

216 As for general DEM, the translation and rotation of each DE in space,  
 217 under resultant force  $\vec{F}$  and torque  $\vec{\Gamma}$  (computed at the center of mass), finally  
 218 follow Newton-Euler equations for rigid bodies with  $\vec{v}$  and  $\vec{\omega}$  the linear and  
 219 angular velocities:

$$m \frac{d\vec{v}}{dt} = (1 \pm D) \vec{F} \quad (27)$$

$$\mathbf{I} \frac{d\vec{\omega}}{dt} + \vec{\omega} \wedge \mathbf{I} \vec{\omega} = (1 \pm D) \vec{\Gamma} \quad (28)$$

220 The above Newton-Euler equations are classically damped using a numerical  
 221 coefficient  $D$ , which modifies the resultant force and torque so that kinetic

222 energy always decreases (or is led to increase by a smaller extent) as soon as  
 223  $\vec{F} \neq \vec{0}$ . Eq. (28), relating the variation in  $\vec{\omega}$  with  $\vec{\Gamma}$ , is expressed in local axes  
 224 where the inertia tensor  $\mathbf{I}$  is constant. Denoting  $\mathbf{R}(t)$  the rotation matrix  
 225 passing from local axes to global ones, and  $\mathbf{\Omega}$  the antisymmetric matrix such  
 226 that  $\mathbf{\Omega} \vec{x} = \vec{\omega} \wedge \vec{x}, \forall \vec{x}$ , Eq. (28) is finally supplemented with:

$$\frac{d\mathbf{R}}{dt} = \mathbf{R}\mathbf{\Omega} \quad (29)$$

227 These equations (27)-(29) are then integrated over the time steps through an  
 228 explicit algorithm common to any non-spherical shape in YADE (Šmilauer  
 229 et al., 2015).

## 230 4. Proposed implementation

### 231 4.1. Source code

232 The present C++ and Python implementation inserts LS-DEM into the  
 233 2020.01a version, i.e. the `git` commit 9964f53, of the YADE platform (Šmilauer  
 234 et al., 2015). Figure 3 illustrates the LS-DEM workflow exposed in the previ-  
 235 ous section together with the most noticeable new (or modified) C++ classes  
 236 responsible for execution.

237 Looking from the `lsYade` root folder of the proposed source code, the files  
 238 `pkg/dem/LevelSet.*pp` introduce the new shape descriptor `LevelSet`. That  
 239 class includes the discrete distance field as a `LevelSet.distField` attribute.  
 240 The regular grid carrying the distance field is `LevelSet.lsGrid`, which is  
 241 an instance of the `RegularGrid` class. Boundary nodes are stored in `Lev-`  
 242 `elSet.boundNodes` and computed (once, at the beginning of a simulation)  
 243 solving for cubic roots during the ray tracing procedure mentioned in the  
 244 above Section 3.1. A Newton-Raphson algorithm proposed by the external  
 245 `Boost.Math` library is adopted for this purpose, being preferred over canoni-  
 246 cal formulae for numerical stability. Moreover, the distance cubic polynomial

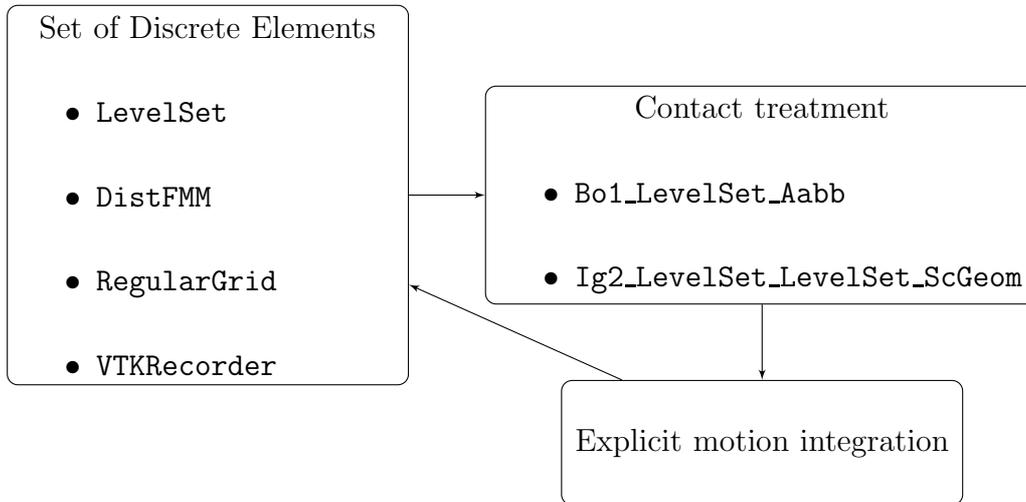


Figure 3: New or modified C++ classes for a LS-DEM workflow in YADE

247 is first turned dimensionless (with respect to the grid spacing) for the relative  
 248 magnitude of its coefficients to be unaffected by the unit system, insuring a  
 249 constant behavior of the root finding algorithm whatever the user's choice in  
 250 this aspect. It is recalled the distance field, its grid and the boundary nodes  
 251 all refer to a reference local (inertial) frame for each particle.

252 The distance field at the heart of the shape descriptor can be directly  
 253 passed from the user (see next section) or also obtained from the Fast March-  
 254 ing Method proposed in `DistFMM` class. In the latter case, `DistFMM.phi()`  
 255 is to execute once the grid and the boundary conditions are defined as `grid`  
 256 and `phiIni` class attributes, respectively. Various predefined functions are  
 257 proposed to build appropriate boundary conditions expected in `phiIni`. In  
 258 addition to a `distIniSE` function intended to compute the distance to su-  
 259 perquadric shapes detailed in Section 5.1, a versatile `PhiIniPy` function may  
 260 be based upon any user-defined Python function that discriminates between  
 261 the inside and the outside of a surface and outputs boundary condition values  
 262 for the FMM, such as shown in Figure 1.

263 Visualization of `LevelSet`-shaped bodies relies on `vtk` exports of the dis-  
264 crete distance field for each DE in current configuration, thanks to a modified  
265 version of files `pkg/dem/VTKRecorder.*pp`. Actual display is typically done  
266 from Paraview software (Ayachit, 2019), using its Python interface and a pro-  
267 vided `pvVisu` function defined in `examples/levelSet/pvVisu.py`. For the  
268 purpose of alternate visualization methods at the user’s discretion, a `Lev-`  
269 `elSet.marchingCubes` method is also available from YADE interface and  
270 gives a triangulated description of a particle’s surface as per the Marching  
271 Cubes algorithm (Lorensen and Cline, 1987).

272 The files `pkg/dem/LevelSetInteraction.*pp` finally implement the con-  
273 tact algorithms described in previous Section 3.2. The `Bo1_LevelSet_Aabb`  
274 is first responsible to compute an axis-aligned bounding box (`Aabb`) used  
275 in YADE for a first, crude and fast, detection of possible contacts. At the  
276 beginning of a simulation, that class first loops over the whole distance field  
277 to compute the 8 corners of the corresponding `Aabb` in local axes, stored  
278 in `LevelSet.corners`. Then, the current `Aabb` in model (global) axes is  
279 easily determined following rigid transformations. In case of overlap between  
280 `Aabb`, precise contact detection subsequently resorts to the other class `Ig2_-`  
281 `LevelSet_LevelSet_ScGeom`, that implements the master-slave contact de-  
282 tection based on boundary nodes, identifying the contact point, if any, and  
283 the associated kinematic variables (normal vector, interpenetration depth)  
284 between two `LevelSet`-shaped bodies. Similar classes enable contact inter-  
285 action between a `LevelSet`-shaped body and existing `Wall` or `Box` shapes,  
286 often adopted in YADE to simulate rigid boundaries.

287 In the end, the set of kinematic variables for a LS-DEM interaction is  
288 equivalent in nature to those used for spheres in general DEM and it can  
289 be stored in the existing `ScGeom` class. Constitutive properties  $k_n$ ,  $k_t$  and  $\mu$

290 also correspond to the pre-existing `FriictPhys` contact model in YADE. This  
291 enables LS-DEM simulations to adopt a pre-existing contact law, namely  
292 `Law2_ScGeom_FriictPhys_CundallStrack`. Motion integration as described  
293 in previous Section 3.3 has also been readily available from the `NewtonIn-`  
294 `tegrator` class.

#### 295 *4.2. Code usage*

296 The (modified or classical) YADE platform starts in the form of a Python3  
297 interactive interface, invoked from `install/bin/yadelevelSet` in the pro-  
298 posed installation procedure (see the “Computer code availability” section).  
299 Instead of an interactive session, scripts prepared beforehand can be as  
300 well passed as argument and launched in the same manner than classical  
301 Python scripts. Examples of YADE scripts using the new LS-DEM fea-  
302 tures can be found in the source code at `lsYade/examples/levelSet/*.py`  
303 (`levelSetBody.py` in particular) and also `lsYade/scripts/checks-and-`  
304 `tests/checks/checkLSdem.py`. The latter actually serves as a new regres-  
305 sion test into the YADE platform (Haustein et al., 2017), to insure stability of  
306 the LS-DEM features in the future. These examples illustrate the definition  
307 of `LevelSet` bodies through a new `levelSetBody()` YADE function. That  
308 function proposes level set descriptions of pre-defined analytical shapes (from  
309 boxes and spheres to superellipsoids, see next Section 5), together with the  
310 possibility of a direct assignment of the regular grid with its distance field.  
311 The latter enables users to directly insert any distance field they would have  
312 otherwise acquired, for instance from computed tomography (Vlahinić et al.,  
313 2014). In all cases, grid spacing  $g_{grid}$  is input through a `spacing` attribute  
314 while a `nNodes` attribute of `levelSetBody()` controls the boundary nodes  
315 number  $N_n$ .

316 Documentation can be obtained for any class or attribute in the usual

317 interactive Python manner, typing e.g. `LevelSet?` or `levelSetBody?`. An  
 318 HTML version of the documentation can also be built executing `make doc`  
 319 from the compilation folder.

### 320 4.3. Code validation

321 The implementation is first validated for what concerns the FMM in  
 322 `DistFMM` class. Applying the procedure on a sphere of radius  $R$  with a known  
 323 distance field  $\phi^{th}(\vec{x}) = r - R$ , numerical precision can be quantified, looking  
 324 e.g. at the average relative error on all gridpoints (excluding those with  $\phi^{th} =$   
 325 0) or at the relative error at the center, as follows:

$$err_{avg} = \text{average} \left( \left\{ \left| \frac{\phi(\vec{x}_i) - \phi^{th}(\vec{x}_i)}{\phi^{th}(\vec{x}_i)} \right|, \vec{x}_i \mid \phi^{th}(\vec{x}_i) \neq 0 \right\} \right) \quad (30)$$

$$err_{ctr} = \frac{\min(\phi) + R}{R} \quad (31)$$

326 Considering Eq. (30), another average error is also analyzed for the more  
 327 complex flake-like shape previously presented in Figure 1. While no exact  
 328 distance field is known for such a surface, one could attempt a reconstruction  
 329 of its inside/outside function  $f$ , Eq. (13), solving another variant of the  
 330 Eikonal equation, with a non-unit speed, i.e.:

$$\|\vec{\nabla}\phi\| = \|\vec{\nabla}f\| \quad (32)$$

331 By initializing the FMM, close to  $\mathcal{S}$ , with values of  $f$ :  $\phi(\vec{x}_i) = f(\vec{x}_i)$  and  
 332 solving for Eq. (32), one should indeed await  $\phi^{th} = f$  as an exact solution.

333 For these two examples of a FMM application, Figure 4 illustrates how  
 334 the FMM results approach their respective  $\phi^{th}$  with a decreasing grid spacing  
 335  $g_{grid}$  i.e. an increasing grid resolution  $r_g = 2R/g_{grid}$ . While the precision is  
 336 somewhat worse for the flake-like surface, in line with an increasing com-  
 337 plexity of the problem, it always linearly scales with the grid resolution, in  
 338 accordance with the first order expression of  $\vec{\nabla}\phi$  in the numerical method.

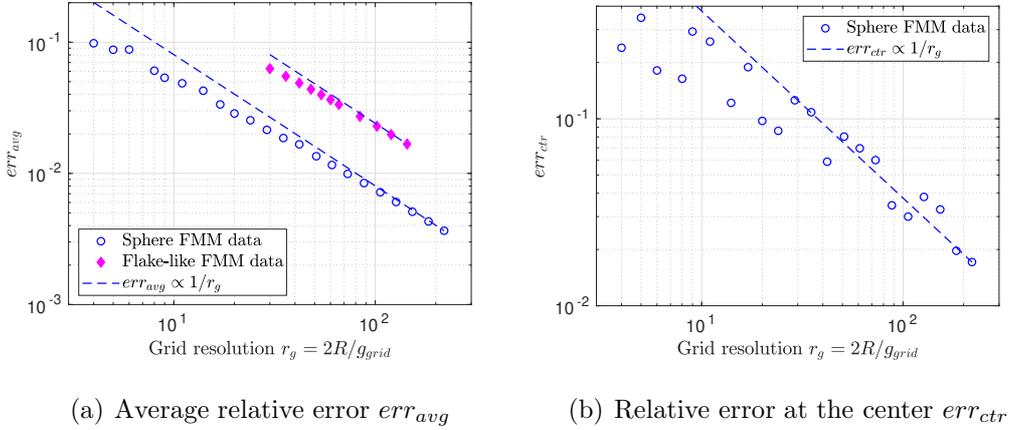


Figure 4: Influence of the grid resolution on the FMM precision, with reference to spherical or flake-like (Figure 1) surfaces

339 Associated time costs are depicted in Figure 5. They refer to distance  
 340 computations, i.e. solving Eq. (8) only, as per the present sequential FMM  
 341 being executed on a workstation having one 4 cores, 8 threads, Intel i7-  
 342 7700, 0.8 - 4.2GHz processor with 8 MB of cache memory, as well as 64  
 343 GB of 2.4 GHz RAM. Each case is run between 3 and 9 times (all depicted  
 344 on the Figure) to account for possible variations in time cost, and after  
 345 using the Linux command `cpufreq` and its `performance` governor set at 4.0  
 346 GHz. Denoting  $N_{gp}$  the total number of gridpoints, with  $N_{gp} = \mathcal{O}(r_g^3)$ , a  
 347  $\mathcal{O}(r_g^6) = \mathcal{O}(N_{gp}^2)$  complexity appears, in accordance with classical Level  
 348 Set Methods. Sethian (1996) actually proposed a lighter complexity for the  
 349 FMM, through adopting a heap sort when searching the minimum  $\phi$ -value  
 350 for propagating the distance field. For the purpose of LS-DEM, the FMM  
 351 will apply only once per DE, at the very beginning of a simulation and the  
 352 present time cost in the order of a second for few tens of grid voxel per particle  
 353 length is actually acceptable, considering the final time cost of a complete  
 354 LS-DEM simulation. Figure 5 finally illustrates that the FMM computation

355 of distance for the more complex, non-spherical, flake-like shape logically  
 356 shows the same time costs.

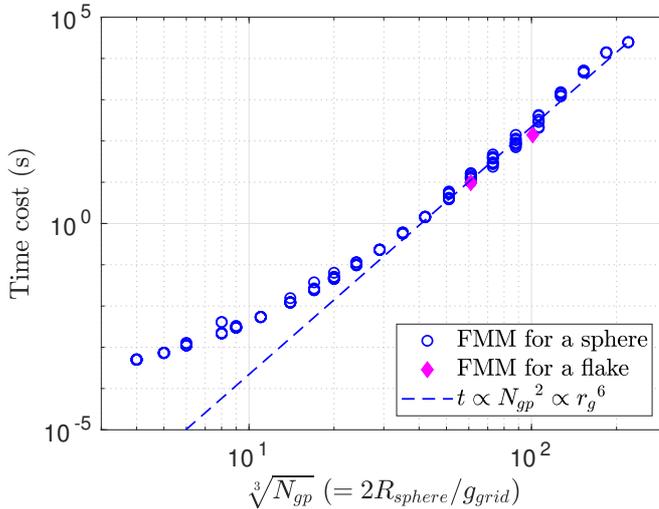


Figure 5: Time cost of the FMM according to the number of gridpoints per space axis  $\sqrt[3]{N_{gp}}$ , with  $N_{gp}$  the total number

357 FMM distance computations aside, code implementation was previously  
 358 validated checking LS-DEM simulations of spherical particles did correspond  
 359 with classical DEM simulations, provided that grid resolution and boundary  
 360 nodes are appropriately chosen (Duriez and Galusinski, 2020; Duriez and  
 361 Bonelli, 2021).

## 362 5. A direct application of LS-DEM to superquadric shapes

363 The versatility of LS-DEM to address complex shapes is now illustrated  
 364 on superellipsoids, also known as superquadric ellipsoids. These surfaces are  
 365 first presented from an analytical point of view before that their LS-DEM de-  
 366 scription is introduced with its corresponding precision and eventually com-  
 367 pared with the possible use of convex polyhedra.

368 *5.1. Superellipsoids surfaces*

369 Superellipsoids (Barr, 1981, 1995) form a versatile class of surfaces which  
 370 can be used as more complex shape models of granular soils (see e.g. Wang  
 371 et al., 2019). They generalize ellipsoids through two additional exponents  $\epsilon_e$   
 372 and  $\epsilon_n$  that enter their surface equation together with three different radii  
 373  $r_x, r_y, r_z$ . In a local frame, the surface equation namely reads:

$$f(x, y, z) = \left( \left| \frac{x}{r_x} \right|^{\frac{2}{\epsilon_e}} + \left| \frac{y}{r_y} \right|^{\frac{2}{\epsilon_e}} \right)^{\frac{\epsilon_e}{\epsilon_n}} + \left| \frac{z}{r_z} \right|^{\frac{2}{\epsilon_n}} - 1 = 0 \quad (33)$$

374 Figure 6 illustrates five different superellipsoids, with their corresponding  
 375 shape parameters presented in Table 1. Table 2 also details their volume and  
 376 inertia properties, as obtained from closed form expressions given by Barr  
 377 (1995). One can here observe how the  $\epsilon_n$  exponent modifies the  $z$ -variation of  
 378 cross-sections in  $(x, y)$  planes. For instance, adopting  $\epsilon_n \rightarrow 0$  induces fairly  
 379 constant cross-sections and a wider distribution of matter for extreme values  
 380 along the “north-south” axis  $\vec{z}$ , see Shapes A or C. On the other hand, the  
 381  $\epsilon_n = 1$  case corresponds to a rounded variation of these cross sections when  
 382 progressing along  $\vec{z}$  (Shape B). Some singularity, i.e. a sharpness at  $z = 0$ ,  
 383 would appear for  $\epsilon_n \geq 2$ , alongside concavity in a plane tangent to  $\vec{z}$  for  
 384  $\epsilon_n > 2$ . For a given  $\epsilon_n$ ,  $\epsilon_e$  controls the contour’s roundness in the  $(x, y)$  plane  
 385 of these cross-sections. While  $\epsilon_e = 1$  corresponds to perfectly round (circles  
 386 or ellipses) contours, decreasing  $\epsilon_e$  towards 0 induce edges that tend to align  
 387 with the  $\vec{x}$  and  $\vec{y}$  axes, see Shape A vs C. Alternate edges and sharpnesses  
 388 would be obtained in the  $(x, y)$  plane at  $\epsilon_e = 2$ , just before concavity in that  
 389 plane, for  $\epsilon_e > 2$ .

390 *5.2. LS-DEM description of superellipsoids*

391 Previous DEM descriptions of superellipsoids have already been proposed  
 392 by Podlozhnyuk et al. (2017) or Weinhart et al. (2020), for instance. In those

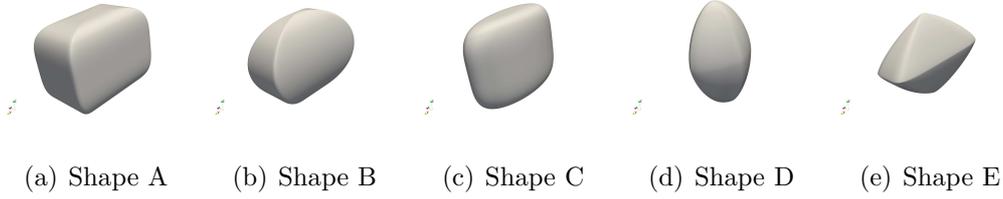


Figure 6: Five possible superquadric shapes

Shape	Half-extents (cm)			Curvature exponents	
	$r_x$	$r_y$	$r_z$	$\epsilon_e$	$\epsilon_n$
A	0.58	1	0.83	0.1	0.5
B	0.42	1	0.83	0.1	1
C	same as Shape B			1	0.5
D	0.5	0.7	1	1.4	1.2
E	0.4	1	0.8	0.4	1.6

Table 1: Shape parameters of the five superellipsoids shown in Figure 6

Shape	Volume (cm <sup>3</sup> )	Inertia components (cm <sup>5</sup> )		
	$V^{th}$	$I_{xx}^{th}/\rho$	$I_{yy}^{th}/\rho$	$I_{zz}^{th}/\rho$
A	3.353	1.649	0.9751	1.358
B	1.852	0.7456	0.3417	0.5770
C	1.914	0.7996	0.4389	0.5153
D	1.093	0.2773	0.2350	0.1304
E	1.086	0.1283	0.3184	0.2625

Table 2: Geometric properties of the considered superellipsoid shapes. Inertia components are obtained following Barr (1995)

393 studies, contact detection involves a minimization procedure that endows  
 394 the shape equation (33) with an approximated distance nature, following  
 395 the potential approach by Houlsby (2009). Such a minimization is then  
 396 performed by an iterative numerical method, at each DEM iteration. On the  
 397 other hand, the generic workflow of LS-DEM is herein proposed to directly  
 398 apply to superquadrics, considering true distance quantities and avoiding the  
 399 need for an iterative procedure, outside the consideration of boundary nodes.

400 The LS-DEM description of a superellipsoid particle nevertheless logically  
 401 shows a finite precision, with for instance the inertial quantities depending  
 402 on the chosen resolution for the grid carrying  $\phi$ , as per the above Section 3.1.  
 403 Quantifying now the grid resolution as  $r_g = 2 \min(r_x, r_y, r_z)/g_{grid}$ , Figure 7  
 404 then compares the obtained LS-DEM volume with the expected volume pre-  
 405 sented in Table 2. It shows that using at least ten grid cells per particle's  
 406 length leads to satisfactory results with an error on the volume being smaller  
 407 than few %. A similar precision is achieved for inertia components, as shown  
 408 in Figure 15 in the Appendix. While this analysis is merely geometric in na-  
 409 ture, a direct connection between errors in describing particles' volumes and  
 410 bias in mechanical results was proposed by Mede et al. (2018) when using  
 411 clumps.

412 The influence of grid spacing on inertial quantities directly relates to the  
 413 voxelised nature of the present description of particle's volume, in connection  
 414 with the sign of discrete  $\phi$ -values  $\phi(\vec{x}_i)$ . Section 4.3 previously illustrated how  
 415 the grid spacing also affects the precision in the actual values of those, after  
 416 solving through a FMM the Eikonal equation. A last impact of grid spacing  
 417 onto the LS-DEM precision exists through the tri-linear interpolation used to  
 418 evaluate distance at any location other than a gridpoint, such as a boundary  
 419 node for the purpose of contact detection. From the present and past results

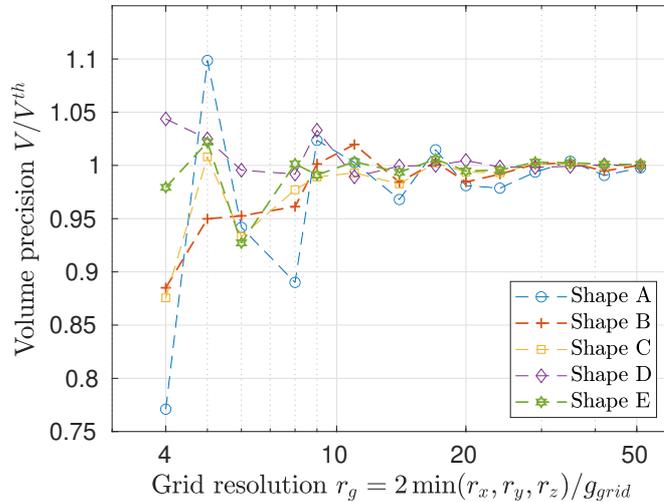


Figure 7: LS-DEM precision in describing superellipsoid volumes, with reference to Figure 6

420 (Duriez and Galusinski, 2020; Duriez and Bonelli, 2021), using  $r_g$  in the  
 421 order of few tens (10 to 50) appears to be an adequate compromise between  
 422 precision and computational (memory) costs, on all aspects.

### 423 5.3. Time costs in comparison with convex polyhedra

424 LS-DEM time costs are now briefly illustrated in comparison with the use  
 425 of convex polyhedra as initially implemented in the YADE platform by Eliáš  
 426 (2014). Describing such `Polyhedra` shapes in YADE relies on the CGAL  
 427 library, used here in its 4.11 version (Kettner, 2018). That external library  
 428 determines for instance a possible overlapping volume between two convex  
 429 polyhedra for the purpose of contact treatment.

430 Such shapes may actually also apply to the present five superellipsoids,  
 431 after locating the polyhedra’s vertices along the superquadric surface. Pre-  
 432 viously determined LS-DEM boundary nodes (with  $r_g = 50$ ) can be used for  
 433 such a purpose. These vertices, through their connecting edges and plane

434 portions (facets) making the polyhedra's surface, govern the precision in de-  
 435 scribing a superellipsoid shape even though, by the present construction, the  
 436 obtained particles volumes are always smaller than the exact volumes of the  
 437 considered (convex) superellipsoids. Figure 8 illustrates how the number of  
 438 vertices controls the obtained volume and the necessity to use hundreds of  
 439 polyhedra vertices in order to limit the error on the volume below few %.

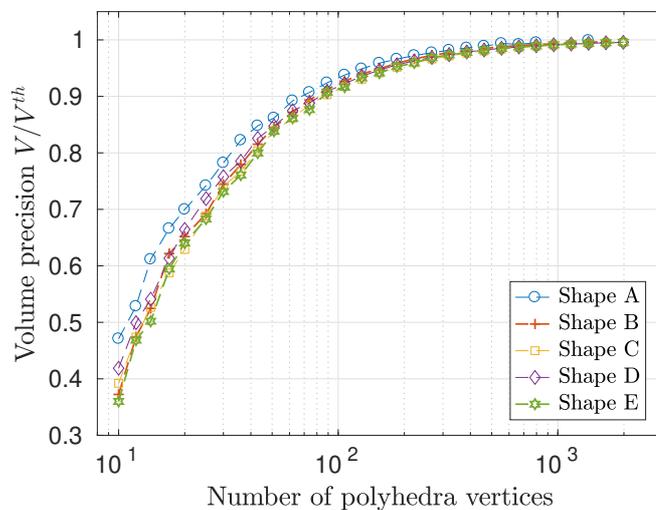


Figure 8: Precision in describing superellipsoid volumes when using convex polyhedra, with reference to Figure 6

440 Comparing the YADE use of `Polyhedra` or `LevelSet` shapes is actually  
 441 not direct since the shape precision in LS-DEM both depends upon grid  
 442 resolution and boundary nodes number, with associated computational costs  
 443 being different in nature: memory requirements only (excluding time cost  
 444 at DE creation) for the former, and time cost mostly for the latter. Convex  
 445 polyhedra on the other hand are solely defined by their number of vertices  $N_v$   
 446 and show virtually no memory requirements. Also, the use of LS-DEM with  
 447  $N_n$  boundary nodes may more often miss contacts than the use of convex  
 448 polyhedra with  $N_v = N_n$ , if one thinks e.g. to possible face-to-face contacts.

449 An imperfect comparison is still proposed looking at the time costs during  
 450 YADE contact treatment in both approaches, i.e. the execution of `Interac-`  
 451 `tionLoop` that embeds either the LS-DEM `Ig2_LevelSet_LevelSet_ScGeom`  
 452 or the CGAL-enabled `Ig2_Polyhedra_Polyhedra_PolyhedraGeom` for poly-  
 453 hedra, both being responsible for virtually all time cost of each case. Looking  
 454 at the lone pair of two fixed superquadrics illustrated in Figure 9, contact  
 455 being detected in all cases, associated time costs are depicted according to  
 456 boundary nodes or vertices numbers in Figure 10. Those sequential time costs  
 457 are measured on the same workstation used in Section 2.2, repeating 3 times  
 458 each case and excluding initialization costs that appear in particular at the  
 459 first execution of `Ig2_Polyhedra_Polyhedra_PolyhedraGeom`. Correspond-  
 460 ing scripts are provided at `lsYade/examples/levelSet/seContact.py` and  
 461 `lsYade/examples/polyhedra/seContact.py`.

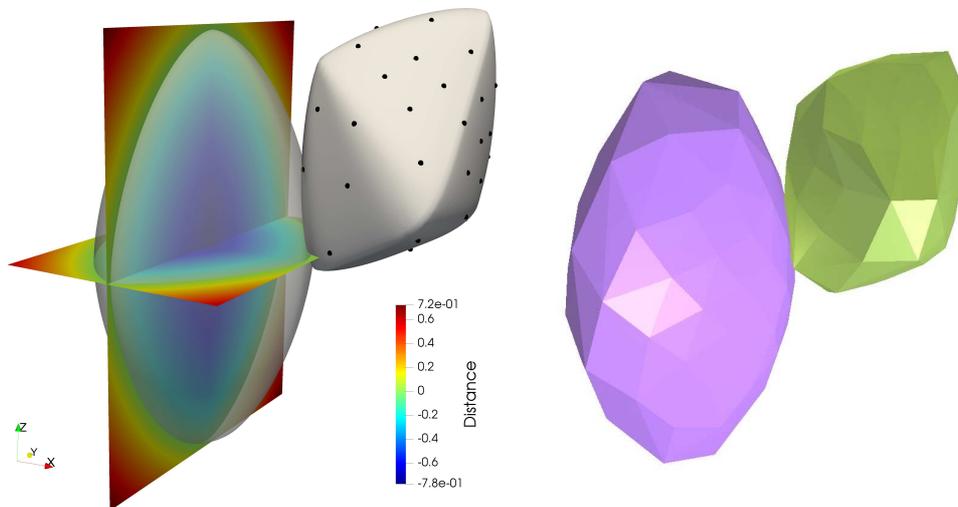


Figure 9: Two contacting superellipsoids described using LS-DEM (left, with 51 boundary nodes) or convex polyhedra (right, with 107 vertices per body)

462 LS-DEM timing data first show a logical proportionality between  $N_n$  and  
 463 time cost  $t$ . Furthermore, the LS-DEM time cost is again shown to be inter-  
 464 estingly insensitive to the grid resolution, even though the latter contributes

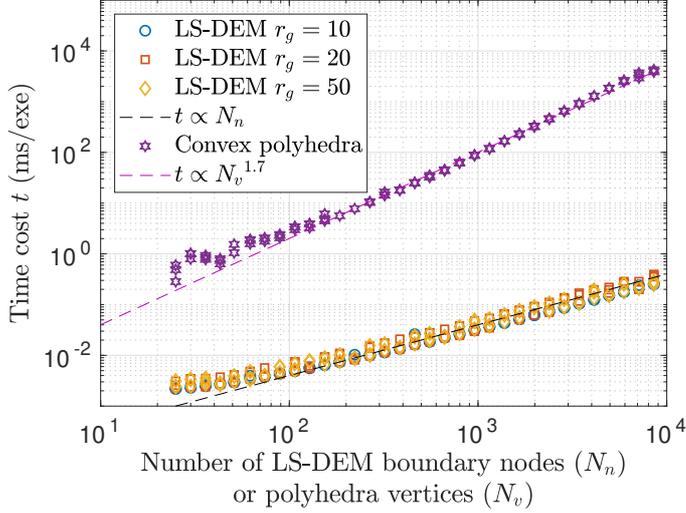


Figure 10: Time costs for computing the single contact of Figure 9 using LS-DEM or convex polyhedra, expressed in milliseconds per execution of `InteractionLoop` in one DEM iteration (see text)

465 to a greater precision. As for the use of convex polyhedra, the corresponding  
466 time cost appears as proportional to  $N_v^{1.7}$ , then close to  $\mathcal{O}(N_v^2)$ . With  $N_v$   
467 being checked to be itself proportional to the number of edges,  $N_e$ , or pla-  
468 nar facets,  $N_f$ , making up each polyhedral surface, this  $\mathcal{O}(N_v^2) = \mathcal{O}(N_e^2)$   
469 time complexity is actually consistent with the consideration of all possible  
470 edge pairs adopted by Eliáš (2014) for that contact algorithm. Mostly, the  
471 polyhedral time cost is several orders of magnitude higher than its LS-DEM  
472 counterpart for  $N_n = N_v$ . In spite of the incomplete equivalence between  $N_n$   
473 and  $N_v$ , these important differences in time costs clearly suggest LS-DEM  
474 might be lighter to use in terms of time, especially if a high fidelity is de-  
475 sired at the particle scale since this would here require hundreds of polyhedra  
476 vertices (Figure 8).

477 **6. Discharge example**

478 *6.1. Simulation setup*

479 A final illustration of LS-DEM is proposed in `examples/levelSet/discharge.py`  
480 as the discharge under gravity ( $\vec{g} = -g\vec{z}$ , with  $g = 9.8\text{m/s}^2$ ) and into a rigid  
481 container ( $L_x \times L_y \times L_z = 0.25^2 \times \infty \text{ m}^3$ ) of  $n_{DE} = 1000$  superellipsoids with  
482 equal proportions of the previous five shapes A to E (Figure 11). Similar  
483 dynamic simulations could serve to study rock falls and slides up to an ob-  
484 stacle, or the angle of repose of granular geomaterials conveyed in industrial  
485 processes.

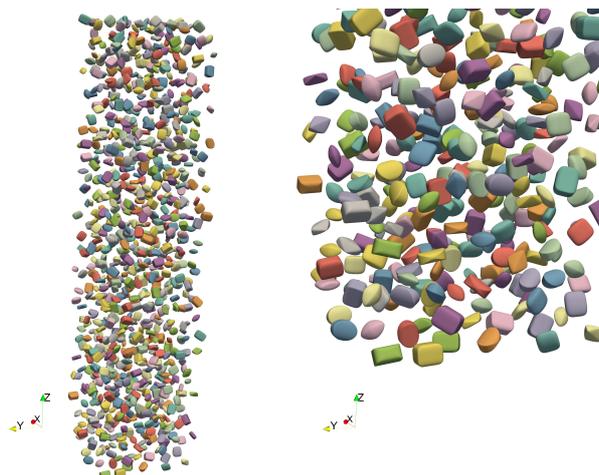


Figure 11: Views of the initial cloud of superellipsoids (left: in whole, right: close-up), with lateral and ground walls of the container not shown

486 In the present simulation, particles initially adopt random orientations  
487 and form a cloud with no contacts: initial porosity is  $n_0 \approx 0.96$  in a  $L_x \times$   
488  $L_y \times L_z = 0.23^2 \times 0.91 \text{ m}^3$  volume. This initial set up is kept the same  
489 for all presented simulations. Table 3 lists the simulation's parameters, with  
490 contact parameters arbitrarily chosen among classical DEM choices, e.g.  $k_n \in$   
491  $\{3 \times 10^4; 3 \times 10^6\} \text{ N/m}$  in (Kawamoto et al., 2016, 2018).

Contact properties			Density	Timestep	Damping
$k_n$	$k_t/k_n$	$\mu$	$\rho$	$\Delta t$	D
(N/m)	(-)	(-)	(kg/m <sup>3</sup> )	( $\mu$ s)	(-)
$10^5$	0.7	$\tan(25^\circ)$ or 0 (lateral walls)	2650	25 $\approx 0.15 \sqrt{\frac{m_{min}}{k_{max}}}$	0.3

Table 3: LS-DEM parameters for the discharge simulation

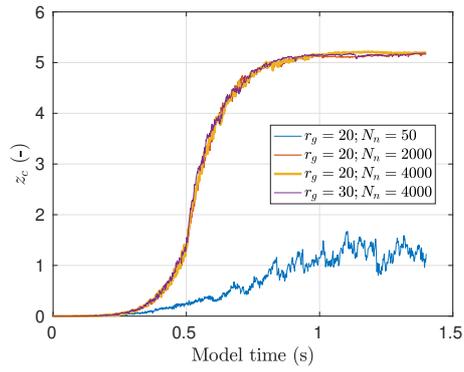
492 *6.2. Results*

493 After executing 56 000 DEM iterations over 1.4 s of model time, a final  
494 equilibrium state can be observed in Figure 12, for what concerns the average  
495 coordination number  $z_c$  or the vertical load exerted on the ground wall  $F$ ,  
496 compared in a  $F^{rel}$  ratio with the expected weight  $F^{th}$  that corresponds to  
497 the theoretical solid volumes of all particles (Table 2):

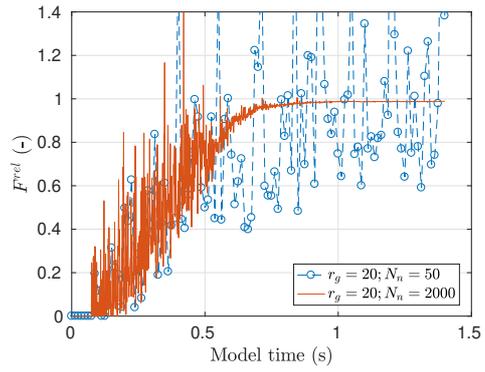
$$F^{rel} = \frac{F}{\rho \|\vec{g}\| \sum_{i=1}^{n_{DE}} V^{th}(i)} \quad (34)$$

498 In this illustrative simulation, most dissipation of the initial gravitational  
499 energy is artificial, coming from the numerical damping mentioned in the  
500 above Section 3.3 used with  $D = 0.3$ .

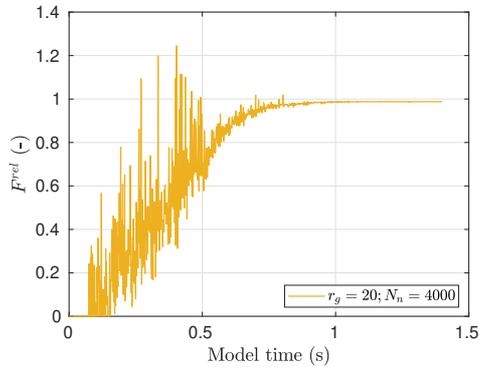
501 Figure 12 also illustrates the possible influence of LS-DEM discretization  
502 parameters  $N_n$  and  $r_g$ . Using just  $N_n = 50$  boundary nodes, together with  
503  $r_g = 20$ , for instance prevents stabilization because contacts are hardly de-  
504 tected and too easily lost. On the other hand, choosing ( $r_g = 20$ ;  $N_n = 2000$ )  
505 here appears as optimal since finer particle descriptions eventually lead to  
506 the same results though with higher computational costs, as discussed in the  
507 following.



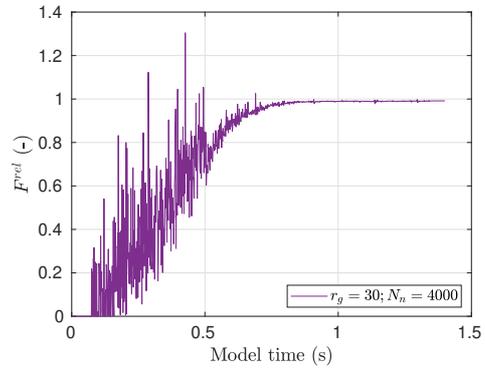
(a)  $z_c$



(b)  $F^{rel}$



(c)  $F^{rel}$  (cont.)



(d)  $F^{rel}$  (cont.)

Figure 12: Dynamics of the discharge illustration (with only a fraction of datapoints for the  $r_g = 20; N_n = 50$  case on (b), for readability)

508 *6.3. Computational costs*

509 Memory (RAM) requirements for LS-DEM simulations are first quantified  
 510 calling the `resource.getrusage` Python function before and after defining  
 511 all DEs. In accordance with the double precision of the present YADE simu-  
 512 lations, used memory is verified in Figure 13 to follow (within a 15% margin)  
 513 a 8 bytes requirement for each scalar value: one for the distance at each  
 514 gridpoint and three for each boundary node (its coordinates). Significant  
 515 memory costs are obtained, being in the order of MB per DE definition. To-  
 516 tal values for the whole simulation in the four cases of Figure 12 are also  
 517 listed in Table 4. It is to note though that those memory requirements could  
 518 be reduced in the future, adopting octree structures to carry the distance  
 519 field instead of regular grids (Duriez and Galusinski, 2020).

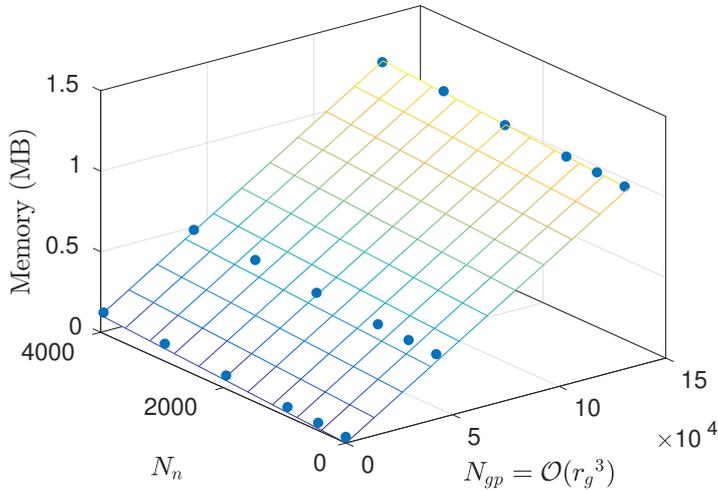


Figure 13: LS-DEM memory requirements per discrete element definition. Each data point is obtained from a different discharge simulation. The planar fit is colored according to memory (also on the  $z$ -axis) and is obtained after bilinear regression, following the expression  $a \times N_{gp} + b \times N_n$  with  $a = 0.0841 \times 10^{-4}$  MB and  $b = 0.2637 \times 10^{-4}$  MB

520 As for execution time, users may expect from the previous Section 5.3

Simulation	RAM usage (MB)
$r_g = 20; N_n = 50$	578
$r_g = 20; N_n = 2000$	625
$r_g = 20; N_n = 4000$	672
$r_g = 30; N_n = 4000$	1391

Table 4: Total (whole simulation) RAM usage for the discharge simulations of Figure 12

521 lighter LS-DEM costs with respect to polyhedra, even though those costs  
522 would logically be even more reduced with ideal spherical shapes (Duriez  
523 and Bonelli, 2021). Time costs can anyway be significantly decreased using  
524 simple OpenMP parallel computing in a shared memory paradigm. Doing  
525 so, loops over interactions (for contact treatment in `InteractionLoop`) or  
526 bodies (for motion integration in `NewtonIntegrator`) are split into differ-  
527 ent OpenMP threads which are simultaneously executed by different CPU  
528 cores. With respect to the sequential case, additional supervisory opera-  
529 tions become necessary in order to avoid simultaneous access to the same  
530 variable in memory from different threads. Nevertheless, OpenMP execution  
531 of the present discharge simulation, using the optimal choices  $r_g = 20$  and  
532  $N_n = 2000$ , appears as very beneficial, with a significant, linear and nearly  
533 optimal, speedup as depicted in Figure 14. Speedup is here measured re-  
534 peating 3 times each parallel execution as well as the sequential one, on a  
535 server machine with two Intel Xeon Platinum 8270, 2.7 GHz, processors with  
536 26 cores and 36 MB of cache memory each, i.e. a total of 52 cores and 104  
537 threads, together with 1.5 TB 2.9 GHz RAM. From all these simulations, 9  
538 parallel / sequential timing ratios are computed and depicted in Figure 14  
539 through their average and standard deviation.

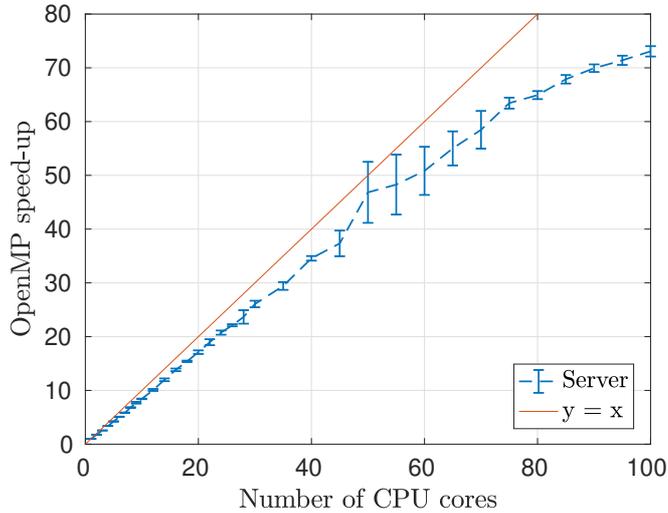


Figure 14: OpenMP scalability of the LS-DEM discharge simulation for  $r_g = 20$  and  $N_n = 2000$ . Sequential time cost is  $28696 \text{ s} \pm 106 \text{ s}$  ( $\approx 8 \text{ h}$ ) from average and standard deviation on 3 runs, being reduced to  $392 \text{ s} \pm 5 \text{ s}$  ( $\approx 6.5 \text{ min}$ ) using 100 CPU cores

540 In the case of a quasistatic simulation being executed on the same ma-  
 541 chine, Duriez and Bonelli (2021) evidenced a linear behavior up to 50 cores  
 542 approximately and with a corresponding speedup of more than 20, before  
 543 that speedup may level off and even decrease.

## 544 7. Conclusions

545 Extending DEM for what concerns shape description, LS-DEM has been  
 546 included in the YADE open-source platform for mechanical simulations of  
 547 granular soils and other discrete systems. With distance-to-surface fields  
 548 serving in a discrete fashion as a primary ingredient of the method, the pro-  
 549 posed implementation also includes a Fast Marching Method to construct  
 550 such fields for a wide class of surfaces with an analytical description. The  
 551 versatility of the method is evident from the direct application to superellip-  
 552 soids. On the other hand, significant computational costs are inherent to the

553 method, be it in terms of memory or execution time. Time costs are never-  
554 theless beneficial with respect to a polyhedral description of complex shapes,  
555 as already available in YADE, and they can be furthermore reduced through  
556 OpenMP parallel computing with a significant speed-up. As for the memory  
557 requirements, these could also decrease in the future using a more appro-  
558 priate data structure than the current regular grid (Duriez and Galusinski,  
559 2020).

560 Perspectives lie in user-friendly LS-DEM simulations in YADE for multi-  
561 scale investigations in granular mechanics. A particular multiscale avenue is  
562 formed by the hierarchical modelling approaches where the DEM serves as an  
563 alternative to phenomenological (e.g. elasto-pastic) stress-strain constitutive  
564 relations in structure-scale FEM simulations (e.g. Guo and Zhao, 2014).

## 565 **Appendix**

566 Confirming the analysis made on volumes in Section 5.2 (Figure 7), Fig-  
567 ure 15 illustrates how LS-DEM achieves to describe inertia components of  
568 superellipsoids with a very good precision, provided the grid resolution is fine  
569 enough i.e. includes more than 10 grid voxels per particle length.

## 570 **Conflict of Interest**

571 We wish to confirm that there are no known conflicts of interest associated  
572 with this publication and there has been no significant financial support for  
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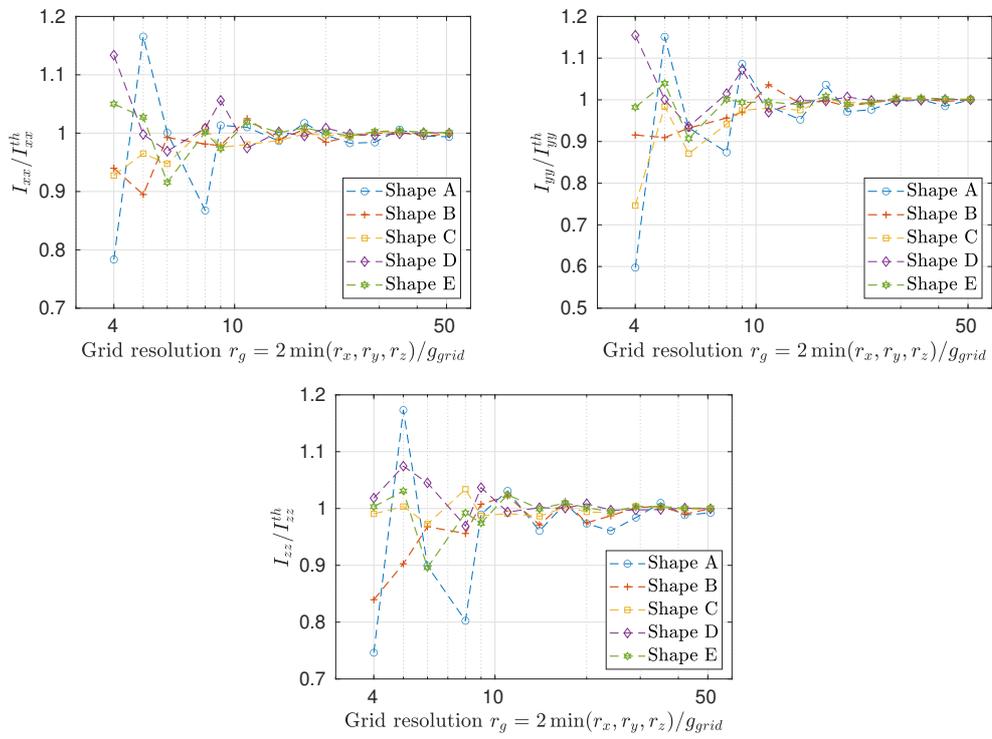


Figure 15: LS-DEM precision in describing inertia components for the five superellipsoids of Figure 6

577 COVER) and Frédéric Golay (Université de Toulon, IMATH) for fruitful dis-  
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579 Computing (“Calcul”). Other YADE developers, passed and present (yade-  
580 dev GitLab team), are also acknowledged for setting up and maintaining the  
581 platform grounding the proposed implementation.

## 582 **Computer code availability**

583 The present LS-DEM code is released under the GNU General Public  
584 License v2. It has been developed by Jérôme Duriez (jerome.duriez@inrae.fr),  
585 the contacting author of the manuscript, and made first available in January  
586 2021.

587 Source code can be currently found at [https://gitlab.com/jduriez/](https://gitlab.com/jduriez/lsYade)  
588 `lsYade`. Insertion into the `master` branch of the YADE platform at [https://](https://gitlab.com/yade-dev/trunk)  
589 [gitlab.com/yade-dev/trunk](https://gitlab.com/yade-dev/trunk) is planned after publication, in addition to the  
590 classical deposit at <https://github.com/CAGEO>.

591 A bash script `install.sh` is for instance available at [https://gitlab.](https://gitlab.com/jduriez/lsYade)  
592 [com/jduriez/lsYade](https://gitlab.com/jduriez/lsYade) and in the manuscript submission, in order to down-  
593 load source code and trigger compilation. After a correct installation, execut-  
594 ing `install/bin/yadelevelSet --check` should include running: `checkLS-`  
595 `dem.py [...] Status: success` in its output.

596 YADE LS-DEM simulations are realistically possible on computing-oriented,  
597 multi-core (clock speed higher than 2.5 GHz) personal desktops, with signifi-  
598 cant RAM: several tens of GB are for instance necessary for simulating Rep-  
599 resentative Elementary Volumes of granular soils with an adequate precision.  
600 Visualization of the simulations builds upon the free, open-source, Paraview  
601 software and its Python interface. Compilation dependencies include e.g.  
602 `cmake`, `g++`, `boost`, `Qt`, `freeglut3`, `libQGLViewer`, `eigen`, `gdb`, `sqlite3`, `Loki`,

603 VTK, Python3 including numpy, sphinx, IPython, matplotlib on Ubuntu  
604 18.04 or 20.04 (see the Prerequisites section of `install.sh`. Note that the  
605 Paraview Python interface is provided by `paraview-python`, resp. `python3-`  
606 `paraview`, package on Ubuntu 18.04, resp. 20.04).

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