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# Is diversification a suitable option to reduce drought-induced risk of forest dieback? An economic approach focused on carbon accounting

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#### **Electronic Supplementary Material**

#### 1 Definition of drought occurrences

Drought occurrence events were defined on the basis of daily soil water content as computed by the daily forest water balance model, BILJOU©.

Water balance computations were performed for a representative beech stand of the Grand-Est region with an average site fertility (i.e., available soil water content of 100 mm and leaf area index of 5.5) for the reference climate, RCP 4.5 and RCP 8.5 (data from the ARPEGE model). More precisely, we hypothesized that (i) the soil properties, especially soil extractable water and soil retention curves, and (ii) canopy leaf area index (since management scenarios do not change stand density) would be unchanged in the future. Only climatic forcing was changed according to the RCPs scenario.

The BILJOU© model requires daily climatic input data to compute potential evapotranspiration, including both radiative and convective terms (global radiation, air humidity, wind speed, air temperature) as the driver for stand transpiration requirements. The potential increase in vapor pressure deficit due to temperature increment in climate change scenarios is then taken into account. Daily rainfall is used to compute rainfall interception and throughfall that refills soil water content. Depending on the relative soil water content, canopy transpiration is reduced thanks to a decrease in canopy conductance. A complete description of the model is available in Granier et al. [5] and a flow chart in Granier et al. [4].

#### 2 Simulation of forest management

Simulations were performed as follows. First, inventory data were loaded. Each inventory file contained the tree records of ten plots of 400 m<sup>2</sup> each. Secondly, we used MATHILDE's built-in harvest algorithm to implement the management scenarios. The algorithm requires some bounds in terms of basal area. Whenever the upper bound is crossed, the harvesting (i.e., thinning) is triggered and the trees are harvested until the lower bound is reached. The bounds were assumed to reproduce the management of even-aged and uneven-aged stands (see Table 4). We enabled the recruitment of new trees in uneven-aged stands to keep the forest dynamics going, but not for even-

aged stands, in order to compute one rotation length at a time. In some cases, natural disturbances cause too much damage for the stand to recover. To consider this, we applied a triggering condition whereby if the number of standing trees at any point in time goes below the threshold of 100 trees per hectare, the stand is not deemed viable and it is automatically harvested.

Management scenario	Stand age (years)	Bounds (m <sup>2</sup> /ha)
Even-aged beech stand	0-50	[14, 18]
	50-70	[18, 22]
	70 until final cut	[22, 26]
Even-aged oak stand	0-50	[14, 18]
-	50 until final cut	[18, 22]
Even-aged mixed stand	0-50	[14, 18]
-	50 until final cut	[18, 22]
Uneven-aged beech stand	n/a	[14, 18]
Uneven-aged oak stand	n/a	[12, 16]
Uneven-aged mixed stand	n/a	[12, 16]

**Table 4** Basal area bounds  $(m^2/ha)$  that were used in the different management scenarios (source: CRPF<sup>1</sup>). The bounds are age-dependent for even-aged management scenarios. n/a: not applicable

#### **3** Creation of fictitious stands

We created a fictitious stand for each management scenario. More precisely, the mixed stand of beech and oak used has the same density as the monoculture stand: the introduced species replaces part of the current species in the stand (25, 50 or 75%) without any change in the leaf area index.

Concerning diversification by structure, the stand is defined as a homogeneous uneven-aged stand according to the structure triangle used in the French forest management. It corresponds to the share of stand basal area of three different diameter classes. In our study, stands are composed of roughly 30% of trees with a DBH of 17.5–27.5 cm, 45% of trees with a DBH of 27.5–47.5 cm, and 25% of trees with a DBH of more than 47.5 cm.

#### **4 MATHILDE and CAT**

MATHILDE is an individual-based model that simulates forest dynamics [2]. It is fitted to data from a large network of permanent plots measured over the 1958-2007 period. It is designed to simulate even-aged and unevenaged stands as well as pure and mixed stands of beech and sessile oak in Northern France. More precisely, it predicts tree mortality, the diameter increment of survivors and the recruitment of new trees over five-year growth periods. The model is composed of different submodels, which are illustrated in Fig. 2.

<sup>&</sup>lt;sup>1</sup> Regional Center for Privately-Owned Forests.



Fig. 2 Flowchart of the submodels composing MATHILDE

The climate submodel is fitted to data from the SAFRAN model over the 1958-2012 period. It predicts the mean seasonal temperature over a period, depending on the initial year of the period and the occurrence of extreme drought events during the period. The growing season temperature is controlled by a parameter that drives its increase. This parameter depends on the given climate scenario and changes when an extreme drought event occurs during the period.

The mortality submodel encompasses many explanatory variables such as tree species, diameter at breast height (DBH, 1.3 m in height), basal area of trees with DBH larger than the subject tree, as well as the occurrence of extreme drought events, windstorm and harvesting [8].

The diameter-increment submodel predicts the increment of a given tree over a period [7]. The explanatory variables are tree species, DBH, basal area of trees with DBH larger than the subject tree, plot basal area, harvest occurrence, and mean seasonal temperature during the time interval.

The submodel of tree recruitment predicts the number of trees that cross the threshold of 7.5 cm for each species. This submodel is enabled only in the case of uneven-aged management. The explanatory variables are the all-

species basal area as well as the basal area of the species. In addition to the aforementioned submodels, MATHILDE also includes a model of height-diameter relationships [3].

MATHILDE is implemented on the CAPSIS platform [1], which contains a carbon accounting tool (CAT, [9]). CAT allows for the representation of complex emission life cycles inherent to managed forests. It takes the main issues related to carbon accounting tools into account, such as the numerous uncertainties, risk of carbon leakage and double counting. The assessment of the carbon balance is also supported by built-in Monte Carlo error propagation methods. Simulations are run by default under global warming potential factors of the fifth assessment report on climate change [6]. Results are exported in carbon units with the probability level of the confidence intervals equal to 0.95 by default.

#### 5 Approximation of the LEV by the doubly-weighted LEV

#### 5.1 Derivation of the estimators of LEV

The estimator of the  $\hat{E}[NPV(T)]$  is denoted as follows:

$$\hat{E}[NPV(T)] = \frac{1}{Z} \sum_{z=1}^{Z} NPV(min(H_z, T)).$$
(1)

$\hat{E}[NPV(T)]$	Expectation of the net present value in EUR/ha for the target rotation length $T$
$H_z$	Age at which the exogenous harvesting condition was reached for realization $z$
NPV(T)	Net present value in EUR/ha for the target rotation length T
Т	Target rotation length (i.e., the harvest age) in years
Ζ	Index to denote any given realization
Ζ	Total number of realizations

In a deterministic setting, the LEV can be obtained from the one-single-rotation net present value (NPV), as follows:

$$LEV(T) = \sum_{i=0}^{+\infty} \frac{NPV(T)}{(1+r)^{j.T}} \,.$$
(2)

j	Rotation number
LEV(T)	Land expectation value in EUR/ha for the target rotation length T
NPV(T)	Net present value in EUR/ha for the target rotation length T
r	Discount rate
Т	Target rotation length (i.e., the harvest age) in years

We only have Z Monte Carlo simulations, but we need an infinite number of revolutions to be able to calculate a LEV. In order to calculate an estimator of the LEV, we will therefore assume that we choose an infinite number of times among the Z Monte Carlo simulations. Finally, we can write exactly:

$$\hat{E}[LEV(T)] = \frac{1}{Z} \sum_{z=1}^{Z} \left[ NPV\left(min(H_z, T)\right) + \frac{1}{Z} \cdot \sum_{z'=1}^{Z} \left[ \frac{NPV\left(min(H_{z'}, T)\right)}{(1+r)^{H_z}} + \frac{1}{Z} \cdot \sum_{z''=1}^{Z} \left[ \frac{NPV\left(min(H_{z''}, T)\right)}{(1+r)^{H_z + H_{z'}}} + \cdots \right] \right] \right].$$
(3)

$\hat{E}[LEV(T)]$	Expectation of the land expectation value in EUR/ha for the target rotation length $T$
	length I
$H_z$	Age at which the exogenous harvesting condition was reached for realization z
NPV(T)	Net present value in EUR/ha for the target rotation length T
Т	Target rotation length (i.e., the harvest age) in years
Z	Index to denote any given realization (with z realizations from the first rotation,
	z' from the second one, $z''$ from the third one)
Z	Total number of realizations

At first sight, it seems that it is possible to aggregate (using the properties of geometric series) to find a compact expression for the expected LEV. However, a simulation has to be performed for each rotation length. In other words, the data from the first NPV sum is not the same as the data from the second sum. Therefore, this type of aggregation is not possible.

If we study each of the terms of this sum, we see that the first term is equal to Eq. 1:

$$\frac{1}{Z} \sum_{z=1}^{Z} NPV (min(H_z, T)) = \hat{E}[NPV(T)].$$
(4)

$\hat{E}[NPV(T)]$	Expectation of the net present value in EUR/ha for the target rotation length $T$
$H_z$	Age at which the exogenous harvesting condition was reached for realization $z$
NPV(T)	Net present value in EUR/ha for the target rotation length T
Т	Target rotation length (i.e., the harvest age) in years
Ζ	Index to denote any given realization
Ζ	Total number of realizations

For the second term, after separating the two sums, we obtain:

$$\frac{1}{Z^{2}} \sum_{z=1}^{Z} \sum_{z'=1}^{Z} \frac{NPV \left( \min(H_{z'}, T) \right)}{(1+r)^{H_{z}}} = \left[ \frac{1}{Z} \sum_{z=1}^{Z} \frac{1}{(1+r)^{H_{z}}} \right] \cdot \left[ \frac{1}{Z} \sum_{z'=1}^{Z} NPV \left( \min(H_{z'}, T) \right) \right]$$
$$= \left[ \frac{1}{(1+r)^{H}} \right] \cdot \hat{E} [NPV(T)], \qquad (5)$$

with *H* so that 
$$\left[\frac{1}{(1+r)^{H}}\right] = \left[\frac{1}{Z}\sum_{z=1}^{Z}\frac{1}{(1+r)^{H_{z}}}\right].$$

$\hat{E}[NPV(T)]$	Expectation of the net present value in EUR/ha for the target rotation length $T$
$H_z$	Age at which the exogenous harvesting condition was reached for realization z
NPV(T)	Net present value in EUR/ha for the target rotation length T
r	Discount rate

Т	Target rotation length (i.e., the harvest age) in years
Z	Index to denote any given realization (with z realizations from the first rotation,
	z' from the second one, $z''$ from the third one)
Ζ	Total number of realizations

We therefore obtain the average of the NPV, discounted by the estimator of the average of the discountings.

For the third term, we obtain:

$$\frac{1}{Z^{3}} \sum_{z=1}^{Z} \sum_{z'=1}^{Z} \sum_{z''=1}^{Z} \frac{NPV \left( \min(H_{z''}, T) \right)}{(1+r)^{H_{z}}} = \left[ \frac{1}{Z} \sum_{z=1}^{Z} \frac{1}{(1+r)^{H_{z}}} \right] \cdot \left[ \frac{1}{Z} \sum_{z'=1}^{Z} \frac{1}{(1+r)^{H_{z'}}} \right] \cdot \left[ \frac{1}{Z} \sum_{z''=1}^{Z} NPV \left( \min(H_{z''}, T) \right) \right] \\ = \left[ \frac{1}{(1+r)^{H}} \right]^{2} \hat{E}[NPV(T)] .$$
(6)

$\hat{E}[NPV(T)]$	Expectation of the net present value in EUR/ha for the target rotation length $T$
$H_z$	Age at which the exogenous harvesting condition was reached for realization $z$
NPV(T)	Net present value in EUR/ha for the target rotation length T
r	Discount rate
Т	Target rotation length (i.e., the harvest age) in years
Ζ	Index to denote any given realization (with z realizations from the first rotation,
	z' from the second one, $z''$ from the third one)
Ζ	Total number of realizations

Iterating this process *ad infinitum*, we obtain:

$$\hat{E}[LEV(T)] = \sum_{i=1}^{+\infty} \hat{E}[NPV(T)] \cdot \left[\frac{1}{(1+r)^{H}}\right]^{j-1}$$

$$= \hat{E}[NPV(T)] \cdot \sum_{i=0}^{+\infty} \left[\frac{1}{(1+r)^{H}}\right]^{j}$$

$$= \hat{E}[NPV(T)] \cdot \frac{(1+r)^{H}}{(1+r)^{H}-1}.$$
(7)

$\hat{E}[NPV(T)]$	Expectation of the net present value in EUR/ha for the target rotation length $T$
$\hat{E}[LEV(T)]$	Expectation of the land expectation value in EUR/ha for the target rotation
	length T
j	Rotation number
r	Discount rate
Т	Target rotation length (i.e., the harvest age) in years

#### 5.2 Numerical intuition and approximation of LEV

In our context of Monte Carlo-based stochastic simulations, there are  $Z^j$  possible LEVs for a given scenario (where Z is the total number of realizations and j the rotation number). Indeed, after the first rotation is terminated (at either age  $H_z$  or age T), a second rotation begins, etc. (Eq. 3).

Let's look at an example to better understand the complexity with only two realizations  $(z_1, z_2)$  and three rotation periods.

In this example, there are eight possible LEVs for a given scenario according to the position of each realization in the time line (first rotation – second rotation – third rotation), as follows:

$z_1 - z_1 - z_1$	$z_2 - z_1 - z_1$
$z_1 - z_2 - z_1$	$z_2 - z_2 - z_1$
$z_1 - z_1 - z_2$	$z_2 - z_1 - z_2$
$z_1 - z_2 - z_2$	$z_2 - z_2 - z_2$

For example, the LEV's calculation for the combination " $z_1 - z_2 - z_1$ " will be as follows:

$$LEV(T) = NPV(min(H_1, T)) + \frac{NPV(min(H_2, T))}{(1+r)^{min(H_1, T)}} + \frac{NPV(min(H_1, T))}{(1+r)^{min(H_1, T) + min(H_2, T)}}.$$
(8)

$H_1$	Age at which the exogenous harvesting condition was reached for realization of
	the first rotation $z_1$
$H_2$	Age at which the exogenous harvesting condition was reached for realization of
	the second rotation $z_2$
LEV(T)	Land expectation value in EUR/ha for the target rotation length T
NPV(T)	Net present value in EUR/ha for the target rotation length T
r	Discount rate
T	Target rotation length (i.e., the harvest age) in years

This example shows the impossibility of calculating the infinite possibilities of LEV for each scenario (i.e., with 1000 realizations and, above all, with an infinite number of rotations). For this reason, we have approximated LEV by integrating an average rotation length  $\overline{H}(T)$  from the second rotation, defined as:

$$\hat{E}[LEV(T)] = \frac{1}{Z} \sum_{z=1}^{Z} \left[ NPV\left(min(H_z, T)\right) + \frac{\hat{E}[NPV(T)]}{(1+r)^{min(H_z, T)}} \frac{(1+r)^{\overline{H}(T)}}{(1+r)^{\overline{H}(T)} - 1} \right],\tag{9}$$

where 
$$\overline{H}(T) = \sum_{z=1}^{Z} \frac{\min(H_z, T)}{Z}$$
. (10)

$\hat{E}[LEV(T)]$	Expectation of the land expectation value in EUR/ha for the target rotation length $T$
$\hat{E}[NPV(T)]$	Expectation of the net present value in EUR/ha for the target rotation length $T$
Hz	Age at which the exogenous harvesting condition was reached for realization z
$\overline{H}(T)$	Mean of the final harvest age in years for the target rotation length $T$
NPV(T)	Net present value in EUR/ha for the target rotation length T
r	Discount rate
Т	Target rotation length (i.e., the harvest age) in years
Z	Index to denote any given realization
Ζ	Total number of realizations

In other words, we are doing the calculation for the combination " $z_1 - z_{mean} - z_{mean}$ ..."

If the number of realizations is large enough, then the mean harvest age  $\overline{H}(T)$  is representative of the theoretical mean, which allows us to compute the mean economic payoff-to-go after the first rotation as  $\widehat{E}[NPV(T)]$ . (1 + r) $\overline{H}(T)/((1 + r)\overline{H}(T) - 1)$ . Indeed, if we computed:

$$\hat{E}[LEV(T)] = \frac{1}{Z} \sum_{z=1}^{Z} \left[ NPV \left( min(H_z, T) \right) + \frac{\hat{E}[NPV(T)]}{(1+r)^{\overline{H}(T)} - 1} \right],$$
(11)

$\hat{E}[LEV(T)]$	Expectation of the land expectation value in EUR/ha for the target rotation length $T$
$\hat{E}[NPV(T)]$	Expectation of the net present value in EUR/ha for the target rotation length T
$H_z$	Age at which the exogenous harvesting condition was reached for realization z
$\overline{H}(T)$	Mean of the final harvest age in years for the target rotation length $T$
Z	Index to denote any given realization
Ζ	Total number of realizations
NPV(T)	Net present value in EUR/ha for the target rotation length T
r	Discount rate
T	Target rotation length (i.e., the harvest age) in years

the approximation error between Eq. 9 and Eq. 11 is under 1% and thus negligible.

#### 6 Land expectation value and sensitivity analysis of discount rate

We performed a sensitivity analysis of the discount rate. The results are presented in Table 5 and are ranked by their economic return (LEV) for each climate scenario. The detailed gain and loss compared to the baseline (Baseline\_B and B\_EA) are provided in Table 6.

**Table 5** Scenario codes ranked from the highest economic return to the lowest one for each climate scenario (reference, RCP 4.5 and RCP 8.5) and for four discount rates (1%, 2%, 3% and 4%). The four tables correspond to LEV considering only timber production (W) (top left) or with carbon storage (W+C) for a carbon value of 28 EUR/tC (top right), 54 EUR/tC (bottom left) and 110 EUR/tC (bottom right). Each management scenario corresponds to a color

W	0.01	0.02	0.03	0.04	W+C_28	0.01	0.02	0.03	0.04
RFF	Baseline_O	Baseline_O	Baseline_O	Baseline_O	RFF	Baseline_O	Baseline_O	Baseline_O	Baseline_O
	Baseline_B	Baseline_B	Baseline_B	Baseline B		Baseline_B	Baseline_B	Baseline_B	Baseline_B
	Mix25_UA	Mix25_UA	Mix25_UA	Mix75_EA		Mix25_UA	Mix25_UA	Mix25_UA	Mix50_EA
	Mix50 UA	Mix50_UA	Mix50 UA	Mix50_EA		Mix50 UA	Mix50_UA	Mix50 UA	Mix75_EA
	B_EA	Mix75 UA	Mix50_EA	Mix25 EA		B_EA	Mix75 UA	Mix50_EA	Mix25 EA
RCP 4.5	Mix75_UA	Mix50_EA	Mix75_EA	Mix25_UA	RCP 4.5	Mix75_UA	Mix50_EA	Mix75_EA	Mix25_UA
	B_UA	Mix75_EA	Mix25_EA	Mix50_UA		B_UA	Mix75_EA	Mix25_EA	Mix50_UA
	Mix50_EA	B_UA	Mix75_UA	Mix75_UA		Mix50_EA	Mix25_EA	Mix75_UA	Mix75_UA
	Mix75_EA	Mix25_EA	B UA	B UA		Mix75_EA	B UA	B UA	B UA
	Mix25_EA	B_EA	B_EA	B_EA		Mix25_EA	B_EA	B_EA	B_EA
	Mix25_UA	Mix25_UA	Mix25_UA	Mix25_EA		Mix25_UA	Mix25_UA	Mix25_UA	Mix25_EA
	Mix50_UA	Mix50_UA	Mix50_UA	Mix25_UA		Mix50_UA	Mix50_UA	Mix50_UA	Mix25_UA
	Mix75_EA	Mix75 UA	Mix25_EA	Mix50_UA		Mix50_EA	Mix75 UA	Mix25_EA	Mix50_UA
RCP 8.5	Mix50_EA	Mix25_EA	Mix75_UA	Mix75_UA	RCP 8.5	B_EA	Mix25_EA	Mix75_UA	Mix75_UA
	B_EA	B_UA	B_UA	B_UA		Mix75_EA	B_UA	B_UA	B_UA
	Mix75 UA	Mix50_EA	Mix50_EA	Mix50_EA		Mix75_UA	B_EA	B_EA	B_EA
	B_UA	B EA	B_EA	B_EA		B_UA	Mix50_EA	Mix50_EA	Mix50_EA
	Mix25_EA	Mix75_EA	Mix75_EA	Mix75_EA		Mix25_EA	Mix75_EA	Mix75_EA	Mix75_EA
W+C 54	0.01	0.02	0.03	0.04	W+C 110	0.01	0.02	0.03	0.04
W+C_54	0.01 Baseline_O	0.02 Baseline_O	0.03 Baseline_O	0.04 Baseline_O	W+C_110	0.01 Baseline_O	0.02 Baseline_O	0.03 Baseline_O	0.04 Baseline_O
W+C_54 REF.	0.01 Baseline_O Baseline B	0.02 Baseline_O Baseline B	0.03 Baseline_O Baseline B	0.04 Baseline_O Baseline B	<u>W+C_110</u> REF.	0.01 Baseline_O Baseline B	0.02 Baseline_O Baseline B	0.03 Baseline_O Baseline B	0.04 Baseline_O Baseline B
W+C_54 REF.	0.01 Baseline_O Baseline B Mix25_UA	0.02 Baseline_O Baseline B Mix25_UA	0.03 Baseline_O Baseline_B Mix25_UA	0.04 Baseline_O Baseline B Mix50_EA	<b>W+C_110</b> REF.	0.01 Baseline_O Baseline B B_UA	0.02 Baseline_O Baseline B Mix25_UA	0.03 Baseline_O Baseline_B Mix25_UA	0.04 Baseline_O Baseline B Mix50_EA
<u>W+C_54</u> REF.	0.01 Baseline_O Baseline B Mix25_UA Mix50_UA	0.02 Baseline_O Baseline B Mix25_UA Mix50_UA	0.03 Baseline_O Baseline B Mix25_UA Mix50_UA	0.04 Baseline_O Baseline B Mix50_EA Mix75_EA	<u>W+C_110</u> REF.	0.01 Baseline_O Baseline B B_UA Mix25_UA	0.02 Baseline_O Baseline B Mix25_UA B UA	0.03 Baseline_O Baseline B Mix25_UA B UA	0.04 Baseline_O Baseline B Mix50_EA Mix75 EA
W+C_54 REF.	0.01 Baseline_O Baseline B Mix25_UA Mix50 UA B EA	0.02 Baseline_O Baseline B Mix25_UA Mix50 UA Mix75_UA	0.03 Baseline_O Baseline B Mix25_UA Mix50_UA Mix50_EA	0.04 Baseline_O Baseline B Mix50_EA Mix75_EA Mix25_EA	<u>W+C_110</u> REF.	0.01 Baseline_O Baseline B B_UA Mix25 UA Mix25 UA	0.02 Baseline_O Baseline B Mix25_UA B UA Mix50 UA	0.03 Baseline_O Baseline B Mix25_UA B UA Mix50 UA	0.04 Baseline_O Baseline B Mix50_EA Mix75_EA Mix25_EA
W+C 54 REF.	0.01 Baseline_O Baseline B Mix25_UA Mix50 UA B EA B UA	0.02 Baseline_O Baseline B Mix25_UA Mix50 UA B UA	0.03 Baseline_O Baseline B Mix25_UA Mix50_UA Mix50_EA Mix75_EA	0.04 Baseline_O Baseline B Mix50_EA Mix75_EA Mix25_EA Mix25_UA	<u>W+C_110</u> REF.	0.01 Baseline_O Baseline B B_UA Mix25 UA Mix50 UA B EA	0.02 Baseline_O Baseline B Mix25_UA B UA Mix50 UA Mix75_UA	0.03 Baseline_O Baseline B Mix25_UA B UA Mix50 UA Mix50 EA	0.04 Baseline_O Baseline B Mix50_EA Mix75_EA Mix25_EA Mix25_UA
W+C 54 REF. RCP 4.5	0.01 Baseline_O Baseline B Mix25_UA Mix50 UA B EA B UA Mix75 UA	0.02 Baseline_O Baseline B Mix25_UA Mix50 UA Mix75 UA B UA Mix50 EA	0.03 Baseline_O Baseline B Mix25_UA Mix50_UA Mix50_EA Mix75_EA Mix25_EA	0.04 Baseline_O Baseline B Mix50_EA Mix25_EA Mix25_EA Mix25_UA	W+C_110 REF. RCP 4.5	0.01 Baseline_O Baseline B B_UA Mix25 UA Mix50 UA B EA Mix75 UA	0.02 Baseline_O Baseline B Mix25_UA B UA Mix50 UA Mix75 UA Mix50 EA	0.03 Baseline_O Baseline B Mix25_UA B UA Mix50 UA Mix50 EA Mix75 EA	0.04 Baseline_O Baseline B Mix50_EA Mix25 EA Mix25 EA Mix25 UA
W+C 54 REF. RCP 4.5	0.01 Baseline_O Baseline B Mix25_UA Mix50_UA B EA B UA Mix75_UA Mix50_EA	0.02 Baseline_O Baseline B Mix25_UA Mix50_UA B UA Mix50_EA Mix75_EA	0.03 Baseline_O Baseline B Mix25_UA Mix50 UA Mix50 EA Mix75 EA Mix25 EA	0.04         Baseline_O         Baseline B         Mix50_EA         Mix75 EA         Mix25 EA         Mix25 UA         Mix50 UA         Mix50_UA	W+C_110 REF. RCP 4.5	0.01         Baseline_O         Baseline B         B_UA         Mix25 UA         Mix50 UA         B EA         Mix75 UA         Mix75 UA	0.02 Baseline_O Baseline B Mix25_UA B UA Mix50 UA Mix50 EA Mix50 EA	0.03 Baseline_O Baseline B Mix25_UA B UA Mix50 UA Mix50 EA Mix75 EA Mix25_EA	0.04         Baseline_O         Baseline B         Mix50_EA         Mix75 EA         Mix25 EA         Mix25 UA         B UA         Mix50_UA
W+C 54 REF. RCP 4.5	0.01 Baseline_O Baseline B Mix25_UA Mix50_UA B EA B UA Mix75_UA Mix50_EA Mix75_EA	0.02 Baseline_O Baseline B Mix25_UA Mix50 UA Mix75_UA Mix50 EA Mix75_EA	0.03 Baseline_O Baseline B Mix25_UA Mix50_UA Mix50_EA Mix75_EA Mix25_EA Mix75_UA B_UA	0.04 Baseline_O Baseline B Mix50_EA Mix25 EA Mix25 EA Mix25 UA Mix50 UA	W+C_110 REF. RCP 4.5	0.01 Baseline_O Baseline B B_UA Mix25 UA Mix50 UA B EA Mix75 UA Mix50_EA Mix75 EA	0.02 Baseline_O Baseline B Mix25_UA B UA Mix50 UA Mix50 UA Mix75_UA Mix75_EA	0.03 Baseline_O Baseline B Mix25_UA B UA Mix50 UA Mix50 EA Mix75 EA Mix25_EA	0.04 Baseline_O Baseline B Mix50_EA Mix25 EA Mix25 EA Mix25 UA B UA Mix50_UA
W+C 54 REF. RCP 4.5	0.01 Baseline_O Baseline B Mix25_UA Mix50 UA B EA B UA Mix75 UA Mix75 EA Mix75 EA	0.02 Baseline_O Baseline B Mix25_UA Mix50 UA B UA Mix50 EA Mix75_EA Mix25_EA B EA	0.03 Baseline_O Baseline B Mix25_UA Mix50 UA Mix50 EA Mix75 EA Mix25 EA B UA B UA	0.04         Baseline D         Baseline B         Mix50_EA         Mix25 EA         Mix25 UA         Mix50_UA         Mix50_UA         BUA         B UA         B EA	W+C_110 REF. RCP 4.5	0.01 Baseline_O Baseline B B_UA Mix25 UA Mix50 UA B EA Mix75 UA Mix75 EA Mix75 EA	0.02 Baseline_O Baseline B Mix25_UA B UA Mix50 UA Mix50 EA Mix50 EA Mix25_EA B EA	0.03 Baseline_O Baseline B Mix25_UA B UA Mix50 UA Mix50 EA Mix75 EA Mix25_EA Mix75 UA B EA	0.04         Baseline O         Baseline B         Mix50_EA         Mix25 EA         Mix25 UA         B UA         Mix50_UA         B UA         Mix75 UA         B EA
W+C 54 REF. RCP 4.5	0.01 Baseline_O Baseline B Mix25_UA Mix50_UA B EA B UA Mix75_UA Mix75_UA Mix75_EA Mix25_EA	0.02 Baseline_O Baseline B Mix25_UA Mix50 UA B UA Mix75_UA Mix50 EA Mix75_EA Mix25_EA B EA	0.03 Baseline O Baseline B Mix25_UA Mix50 UA Mix50 EA Mix75 EA Mix75 UA B UA B UA B EA	0.04         Baseline_O         Baseline B         Mix50_EA         Mix55_EA         Mix25_EA         Mix50_UA         Mix75_UA         B LA         B EA         Mix25_EA	W+C_110 REF. RCP 4.5	0.01         Baseline_O         Baseline B         B_UA         Mix25 UA         Mix50 UA         B EA         Mix50_EA         Mix75 EA         Mix25 EA         B UA	0.02 Baseline D Baseline B Mix25_UA B UA Mix50 UA Mix50 EA Mix75_EA Mix25 EA B EA	0.03 Baseline_O Baseline B Mix25_UA B UA Mix50_EA Mix50_EA Mix75_EA Mix25_EA B EA Mix25_UA	0.04         Baseline_O         Baseline B         Mix50_EA         Mix55_EA         Mix25 EA         B UA         Mix50_UA         Mix50_UA         B UA         Mix75 LA         Mix50_UA         B UA         Mix50_UA         Mix55_UA         Mix55_UA         Mix55_UA         Mix55_UA         Mix55_UA
W+C 54 REF. RCP 4.5	0.01 Baseline_O Baseline B Mix25_UA Mix50 UA B EA B UA Mix75 UA Mix50_EA Mix25 EA Mix25 UA	0.02 Baseline D Baseline B Mix25_UA Mix50 UA B UA Mix50 EA Mix75_EA Mix25_EA B EA Mix25_UA	0.03 Baseline_O Baseline B Mix25_UA Mix50 UA Mix50 EA Mix25 EA Mix25 UA B UA B UA B UA Mix25 UA	0.04         Baseline D         Baseline E         Mix50_EA         Mix25 EA         Mix25 UA         Mix50_UA         Mix50_UA         BUA         BEA         Mix25 EA         Mix50_UA         Mix50_UA         Mix50_UA         Mix50_UA         Mix50_UA         Mix50_UA         Mix50_UA         Mix50_UA         Mix25_UA	W+C_110 REF.	0.01 Baseline D Baseline B B_UA Mix25 UA Mix50 UA Mix75 UA Mix50_EA Mix75 EA Mix25 EA B_UA	0.02 Baseline_O Baseline B Mix25_UA B UA Mix50 UA Mix50 EA Mix75_EA Mix25_EA B EA B UA	0.03 Baseline_O Baseline B Mix25_UA B UA Mix50 UA Mix50 EA Mix75 EA Mix25_EA Mix75 UA B EA Mix25_UA	0.04         Baseline O         Baseline B         Mix50_EA         Mix25 EA         Mix25 UA         B UA         Mix50_UA         B EA         Mix25 EA
W+C 54 REF. RCP 4.5	0.01 Baseline O Baseline B Mix25_UA Mix50 UA B EA D UA Mix75 UA Mix50_EA Mix25 EA Mix25 UA Mix25 UA	0.02 Baseline D Baseline D Mix25_UA Mix50 UA B UA Mix50 EA Mix50 EA B EA Mix25 EA Mix25 UA	0.03 Baseline D Baseline B Mix25_UA Mix50 UA Mix50 EA Mix75 EA Mix25 EA B UA B UA B EA Mix25 UA Mix25 UA	0.04         Baseline D         Baseline B         Mix50_EA         Mix55 EA         Mix25 EA         Mix50 UA         Mix50 UA         B LA         Mix25 EA         Mix50 UA         Mix25 UA         Mix25 LA         Mix25 UA         Mix25 UA         Mix25 UA	W+C_110 REF. RCP 4.5	0.01 Baseline D Baseline B B UA Mix25 UA Mix50 UA Mix50 EA Mix50 EA Mix25 EA B UA Mix25 UA	0.02 Baseline D Baseline B Mix25_UA B UA Mix50 UA Mix50 EA Mix55 EA Mix25 EA B EA B UA	0.03 Baseline_O Baseline B Mix25_UA B UA Mix50 LA Mix50 EA Mix75 EA Mix25_EA Mix25_UA B EA Mix25_UA	0.04         Baseline D         Baseline B         Mix50_EA         Mix55_EA         Mix25 EA         Mix50_UA         B UA         Mix55_UA         Mix50_EA         Mix50_EA         Mix25 EA         Mix50_UA         B UA         Mix55_UA         Mix25_UA         Mix25_UA         B EA         Mix25_UA         B LA         Mix25_UA         Mix25_UA
W+C 54 REF. RCP 4.5	0.01 Baseline O Baseline B Mix25_UA Mix50 UA B EA Mix75 UA Mix50_EA Mix25 EA Mix25 UA Mix25 UA B_UA	0.02 Baseline D Baseline D Mix25_UA Mix50 UA Mix75 UA Mix50 EA Mix75_EA B EA Mix25 UA Mix25 UA Mix50 UA	0.03 Baseline D Baseline D Mix25_UA Mix25_UA Mix50 EA Mix75 EA Mix25 EA B UA B EA Mix25_UA Mix25_UA Mix25_UA	0.04         Baseline D         Baseline B         Mix50_EA         Mix55 EA         Mix25 UA         Mix25 UA         B UA         B EA         Mix25 UA         Mix25 EA         Mix25 UA         Mix50 UA         Mix50 UA	W+C_110 REF. RCP 4.5	0.01         Baseline D         Baseline D         Baseline D         Mix25 UA         Mix50 UA         B EA         Mix50 EA         Mix55 EA         Mix25 EA         Mix25 EA         Mix25 EA         Mix25 UA         Mix25 LA         B UA         Mix25 UA         B UA         B UA         Mix50 UA         B UA         Mix50 UA         B UA         Mix50 UA         B EA	0.02 Baseline D Baseline B Mix25_UA B UA Mix50 UA Mix75 UA Mix75_EA Mix25_EA B EA B UA Mix25_UA Mix25_UA	0.03 Baseline D Baseline B Mix25_UA B UA Mix50 UA Mix50 EA Mix25_EA Mix25_UA B EA Mix25_UA B UA	0.04         Baseline D         Baseline B         Mix50_EA         Mix55_EA         Mix25 LA         Mix25_UA         B UA         Mix50_UA         B UA         Mix55_UA         Mix50_UA         Mix50_UA         Mix55_UA         Mix25_UA         B LA         Mix25_UA         B LA         Mix25_UA         Mix25_UA         B LA         Mix25_UA
W+C 54 REF. RCP 4.5	0.01 Baseline O Baseline B Mix25_UA Mix50 UA B EA Mix50_EA Mix50_EA Mix25 EA Mix25 UA Mix25 UA B_UA	0.02 Baseline D Baseline D Mix25_UA Mix50 UA B UA Mix50 EA Mix25 EA B EA Mix25 UA Mix25 UA Mix25 UA	0.03         Baseline_D         Baseline B         Mix25_UA         Mix50 EA         Mix50 EA         Mix75 EA         Mix25_UA         Mix25_EA         Mix25_UA         Mix25_UA         Mix25_EA         Mix25_UA         Mix25_UA         Mix25_UA         Mix25_UA         Mix50_UA         Mix75_UA         Mix75_UA         Mix75_UA	0.04         Baseline D         Baseline B         Mix50_EA         Mix55 EA         Mix25 UA         Mix50 UA         Mix50 UA         B UA         B EA         Mix25 EA         Mix50 UA         Mix50 UA         Mix50 UA         Mix50 UA         Mix50 UA         Mix25 UA         Mix50 UA	W+C_110 REF. RCP 4.5	0.01         Baseline D         Baseline C         Baseline C         Mix25 UA         Mix50 UA         BEA         Mix50 EA         Mix75 EA         Mix25 EA         Mix25 UA         Mix25 EA         Mix25 LA         Mix25 LA         B UA         B EA         B UA         Mix25 EA         B UA         Mix25 UA         Mix25 UA         B EA         Mix25 UA         Mix25 UA         Mix25 UA         Mix25 UA         Mix25 UA         Mix25 UA         Mix50 UA	0.02         Baseline D         Baseline C         Mix25_UA         B UA         Mix50 UA         Mix50 EA         Mix55 EA         B EA         B UA         Mix25_UA         Mix50 EA         Mix50 EA         Mix25 EA         Mix25 UA         Mix25 UA         Mix25 EA         Mix25 UA         Mix25 UA         Mix25 UA         Mix25 UA         Mix25 UA         Mix25 UA	0.03 Baseline_O Baseline B Mix25_UA B UA Mix50 EA Mix50 EA Mix75 EA Mix25_EA Mix25_UA B EA Mix25_UA B UA	0.04         Baseline D         Baseline B         Mix50_EA         Mix55 EA         Mix25 UA         Mix50_UA         B UA         Mix55 EA         Mix50_UA         Mix50_UA         Mix55 UA         Mix55 UA         Mix50_UA         B EA         Mix25 EA         Mix25 UA         B EA         Mix25 UA         Mix50 UA         Mix50 UA
W+C 54 REF. RCP 4.5	0.01           Baseline_O           Baseline B           Mix25_UA           Mix50_UA           B EA           B UA           Mix50_EA           Mix25_UA           Mix50_EA           Mix25_UA           Mix50_EA           Mix25_UA           Mix25_UA           Mix25_UA           Mix25_UA           Mix25_UA           Mix25_UA           Mix25_UA           Mix50_UA           Mix50_UA           Mix50_UA           Mix50_UA           Mix50_UA           Mix50_UA           Mix50_UA           Mix50_UA           Mix50_UA	0.02 Baseline D Baseline D Mix25 UA Mix50 UA Mix75 UA Mix50 EA Mix25 EA B EA Mix25 UA Mix25 UA Mix25 UA Mix25 UA Mix25 EA	0.03         Baseline_D         Baseline B         Mix25_UA         Mix50_EA         Mix50_EA         Mix75_EA         Mix75_UA         Mix75_EA         Mix75_UA         Mix75_UA         Mix75_UA         Mix75_UA         Mix25_UA         Mix25_UA	0.04         Baseline D         Baseline D         Mix50_EA         Mix55 EA         Mix25 UA         Mix50 UA	W+C_110 REF. RCP 4.5	0.01           Baseline D           Baseline D           Baseline C           Mix25 UA           Mix50 UA           B EA           Mix50 EA           Mix55 EA           Mix25 UA           Mix50 EA           Mix25 EA           Mix25 UA           Mix25 EA           Mix25 UA           Mix25 UA           Mix50 UA           Mix50 EA           Mix50 UA           Mix50 EA           Mix50 EA	0.02 Baseline D Baseline D Mix25_UA D Mix50 UA Mix50 EA Mix75_EA Mix25_EA B EA Mix25_UA Mix25_UA	0.03 Baseline O Baseline D Mix25_UA Mix50 UA Mix50 EA Mix75 EA Mix25_EA Mix25_UA B EA Mix25_UA B UA Mix50 UA	0.04         Baseline D         Baseline B         Mix50_EA         Mix55 EA         Mix25 UA         B UA         Mix50_UA         B UA         Mix55 UA         Mix50_UA         B EA         Mix25 UA         B UA         Mix25 UA         B JUA         Mix25 UA         B JUA         Mix25 UA         B JUA         B JUA         B JUA         Mix25 UA         B JUA         Mix50 UA         B JEA
W+C 54 REF. RCP 4.5	0.01 Baseline D Baseline B Mix25_UA Mix50 UA B EA Mix50 EA Mix55 EA Mix25 EA Mix25 UA Mix25 UA B EA B EA Mix50 EA Mix50 EA	0.02         Baseline_D         Baseline B         Mix25_UA         Mix50 UA         Mix75 UA         Mix75 UA         Mix75 UA         Mix75 UA         Mix50 EA         Mix25 LA         Mix25 UA         Mix25 UA         Mix50 UA         Mix25 EA         Mix25 UA         Mix50 UA	0.03           Baseline D           Baseline C           Mix25_UA           Mix50 EA           Mix75 EA           Mix25_EA           Mix25_UA           Mix25_EA           Mix25_UA           Mix25_EA           Mix25_UA           Mix25_EA           Mix25_UA           Mix25_UA           Mix25_UA           Mix25_UA           Mix25_UA           Mix25_UA           Mix25_EA           Mix75_UA           Mix25_EA           Mix75_UA           Mix75_UA           Mix75_UA           Mix50_UA	0.04         Baseline D         Mix50_EA         Mix55 EA         Mix25 VA         Mix25 VA         Mix50_UA         Mix55 LA         Mix25 VA         Mix25 VA         Mix50 UA         Mix50 VA         Mix50 VA         Mix25 VA         B VA         Mix25 VA         Mix25 VA         B FA         B VA         B EA         Mix50 VA	W+C_110 REF. RCP 4.5	0.01         Baseline D         Baseline C         Baseline C         Baseline C         Mix25 UA         Mix50 UA         Mix50 EA         Mix75 EA         Mix25 EA         Mix25 UA         Mix50 EA         Mix50 EA         Mix50 EA         Mix25 UA         Mix25 EA         Mix25 UA         Mix25 UA         Mix25 UA         Mix50 UA         B EA         Mix50 UA         Mix50 EA         Mix50 EA         Mix50 EA         Mix75 UA	0.02         Baseline_O         Baseline B         Mix25_UA         B UA         Mix50 UA         Mix50 EA         Mix25_EA         B UA         Mix25 CA         Mix25 EA         B UA         Mix25 UA         Mix25 EA         Mix25 UA         Mix25 UA         B UA         Mix25 EA         Mix25 UA         Mix25 UA         B EA         Mix25 UA         Mix25 UA         Mix25 UA         Mix25 UA         Mix50 UA         Mix50 UA	0.03 Baseline D Baseline D Mix25 UA Mix50 UA Mix50 EA Mix75 EA Mix25 EA Mix25 UA B EA Mix25 UA Mix25 UA Mix25 EA Mix25 EA Mix25 EA	0.04         Baseline D         Baseline D         Mix50_EA         Mix55 EA         Mix25 UA         Mix50_UA         Mix50_UA         Mix55 LA         Mix25 KA         Mix50_UA         Mix55 LA         Mix50_UA         B LA         Mix25 UA         B LA         Mix25 UA         B LA         Mix25 UA         B LA         Mix25 UA         B LA         Mix50 UA         B LA         Mix50 UA         B EA         Mix50 UA         B EA         Mix50 EA

**Table 6** Variation of LEV (in terms of percentage) of each scenario compared to the baseline of beech (Baseline\_B or B\_EA), for RCP 4.5 and RCP 8.5 and for four discount rates (1%, 2%, 3% and 4%). The four tables correspond to LEV considering only timber production (W) (top left) or with carbon storage (W+C) for a carbon value of 28 EUR/tC (top right), 54 EUR/tC (bottom left) and 110 EUR/tC (bottom right)

W	Scenarios	0.01	0.02	0.03	0.04	W+C28	Scenarios	0.01	0.02	0.03	0.04
DEE	Baseline_B	-	-	-	-	DEE	Baseline_B	-	-	-	-
KEF.	Baseline_O	211±919	251±234	317±74	376±26	KEF.	Baseline_O	205±944	244±243	313±76	362±26
	B_EA	-	-	-	-		B_EA	-	-	-	-
	Mix25_EA	-83	31	349	1202		Mix25_EA	-78±20	31±4	337±1	1075
	Mix50_EA	-79	40	374	1285		Mix50_EA	-76±21	39±4	365±1	1150
4.5	Mix75_EA	-81	38	372	1287	4.5	Mix75_EA	-76±18	38±3	359±1	1133
RCP	B_UA	-54±78	32±30	154±14	349±8	RCP	B_UA	-54±78	27±30	144±14	304±8
	Mix25_UA	73±466	290±134	622±64	1157±35		Mix25_UA	77±472	274±135	595±64	$1030 \pm 35$
	Mix50_UA	20±341	210±102	483±49	920±27		Mix50_UA	21±346	$197 \pm 103$	461±49	818±27
	Mix75_UA	-40±234	92±74	271±37	552±20		Mix75_UA	-40±239	84±75	257±37	486±20
	B_EA	-	-	-	-		B_EA	-	-	-	-
	Mix25_EA	-33	177	643	1691		Mix25_EA	-41±14	141±2	549	1468
	Mix50_EA	7±366	5±96	3±32	2±12		Mix50_EA	$1 \pm 368$	-1±96	-2±32	-3±12
8.5	Mix75_EA	12±329	-5±88	-17±30	-24±11	8.5	Mix75_EA	-2±331	-17±88	-27±30	-33±11
RCF	B_UA	-22±77	94±31	222±15	391±8	RCF	B_UA	-32±77	69±31	$181 \pm 15$	330±8
	Mix25_UA	230±427	480±124	823±59	1283±32		Mix25_UA	195±433	405±124	$706\pm59$	$1111\pm32$
	Mix50_UA	110±341	360±100	646±49	1026±26		Mix50_UA	82±346	300±101	552±49	886±26
	Mix75_UA	-7±220	179±69	369±35	612±19		Mix75_UA	-19±225	143±69	309±35	523±19
W+C54	Scenarios	0.01	0.02	0.03	0.04	W+C110	Scenarios	0.01	0.02	0.03	0.04
W+C54	Scenarios Baseline B	0.01	0.02	0.03	0.04	W+C110	Scenarios Baseline B	0.01	0.02	0.03	0.04
W+C54 REF.	Scenarios Baseline_B Baseline O	<b>0.01</b> - 199±957	<b>0.02</b> - 241±246	<b>0.03</b> - 308±77	0.04 - 350±26	W+C110 REF.	Scenarios Baseline_B Baseline O	<b>0.01</b> - 186±987	<b>0.02</b> - 234±251	<b>0.03</b> - 284±78	<b>0.04</b> - 322±27
W+C <sub>54</sub> REF.	Scenarios Baseline_B Baseline_O B_EA	<b>0.01</b> - 199±957 -	0.02 - 241±246 -	0.03 - 308±77 -	0.04 - 350±26	W+C110 REF.	Scenarios Baseline_B Baseline_O B_EA	<b>0.01</b> - 186±987 -	<b>0.02</b> - 234±251	0.03 - 284±78 -	0.04 - 322±27
W+C <sub>54</sub> REF.	Scenarios Baseline_B Baseline_O B_EA Mix25_EA	0.01 - 199±957 - -74±44	0.02 - 241±246 - 30±9	0.03 - 308±77 - 326±2	0.04 - 350±26 - 953	W+C110 REF.	Scenarios Baseline_B Baseline_O B_EA Mix25_EA	<b>0.01</b> - 186±987 - -65±95	0.02 - 234±251 - 30±21	0.03 - 284±78 - 259±5	0.04 - 322±27 - 767±1
W+C54 REF.	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA	0.01 - 199±957 - -74±44 -72±43	0.02 - 241±246 - 30±9 39±9	0.03 - 308±77 - 326±2 353±2	0.04 - 350±26 - 953 1020	W+C110 REF.	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA	0.01 - 186±987 - -65±95 -64±90	0.02 - 234±251 - 30±21 37±20	0.03 - 284±78 - 259±5 281±5	0.04 - 322±27 - 767±1 820±1
W+C54 REF.	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA Mix75_EA	0.01 - 199±957 - -74±44 -72±43 -72±37	0.02 - 241±246 - 30±9 39±9 37±7	0.03 - 308±77 - 326±2 353±2 347±2	0.04 - 350±26 - 953 1020 1004	W+C110 REF.	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA Mix75_EA	0.01 - 186±987 - -65±95 -64±90 -64±78	0.02 - 234±251 - 30±21 37±20 36±16	0.03 - 284±78 - 259±5 281±5 276±3	0.04 - 322±27 - 767±1 820±1 808±1
W+C54 REF.	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA Mix75_EA B_UA	0.01 - 199±957 - -74±44 -72±43 -72±37 -16±65	0.02 - 241±246 - 30±9 39±9 37±7 42±26	0.03 - 308±77 - 326±2 353±2 347±2 146±13	0.04 - 350±26 - 953 1020 1004 271±7	W+C110 REF.	Scenarios Baseline_B B_EA Mix25_EA Mix50_EA Mix75_EA B_UA	0.01 - 186±987 - -65±95 -64±90 -64±78 96±45	0.02 - 234±251 - 30±21 37±20 36±16 226±15	0.03 - 284±78 - 259±5 281±5 276±3 403±8	0.04 - 322±27 - 767±1 820±1 808±1 647±5
W+C54 REF.	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA Mix75_EA B_UA Mix25_UA	0.01 - 199±957 - -74±44 -72±43 -72±37 -16±65 79±478	0.02 - 241±246 - 30±9 39±9 37±7 42±26 259±137	0.03 - 308±77 326±2 353±2 347±2 146±13 571±64	0.04 - 350±26 - 953 1020 1004 271±7 910±35	REF.	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA Mix75_EA B_UA Mix25_UA	0.01 - 186±987 - 65±95 -64±90 -64±78 96±45 79±490	0.02 - 234±251 - 30±21 37±20 36±16 226±15 232±140	0.03 - 284±78 - 259±5 281±5 276±3 403±8 453±64	0.04 - 322±27 - 767±1 820±1 808±1 647±5 725±35
W+C54 REF.	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA Mix75_EA B_UA Mix25_UA Mix25_UA	0.01 - 199±957 - -74±44 -72±43 -72±37 -16±65 79±478 20±351	0.02 - 241±246 - 30±9 39±9 37±7 42±26 259±137 186±103	0.03 - 308±77 - 326±2 353±2 347±2 146±13 571±64 442±49	0.04 - 350±26 - 953 1020 1004 271±7 910±35 720±27	W+C110 REF.	Scenarios Baseline_B B_EA Mix25_EA Mix50_EA Mix75_EA B_UA Mix25_UA Mix25_UA	0.01 - 186±987 -65±95 -64±90 -64±78 96±45 79±490 15±361	0.02 - 234±251 - 30±21 37±20 36±16 226±15 232±140 164±105	0.03 - 284±78 - 259±5 281±5 276±3 403±8 453±64 346±50	0.04 - 322±27 - 767±1 820±1 808±1 647±5 725±35 569±27
W+C54 REF.	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA Mix75_EA B_UA Mix25_UA Mix25_UA Mix50_UA	0.01 - 199±957 - -74±44 -72±43 -72±37 -16±65 79±478 20±351 -40±244	0.02 - 241±246 - 30±9 39±9 37±7 42±26 259±137 186±103 77±75	0.03 - 308±77 326±2 353±2 347±2 146±13 571±64 442±49 245±37	0.04 - 350±26 - 953 1020 1004 271±7 910±35 720±27 424±20	RCP 4.5	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA Mix75_EA B_UA Mix25_UA Mix50_UA Mix50_UA	0.01 - 186±987 - 65±95 -64±90 -64±78 96±45 79±490 15±361 -43±256	0.02 - 234±251 - 30±21 37±20 36±16 226±15 232±140 164±105 64±77	0.03 - 284±78 - 259±5 281±5 276±3 403±8 453±64 346±50 184±37	0.04 - 322±27 - 767±1 820±1 808±1 647±5 725±35 569±27 328±20
W+C54 REF.	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA Mix75_EA B_UA Mix25_UA Mix25_UA Mix50_UA Mix75_UA	0.01 - 199±957 - 74±44 -72±43 -72±37 -16±65 79±478 20±351 -40±244	0.02 - 241±246 - 30±9 39±9 37±7 42±26 259±137 186±103 77±75 -	0.03 - 308±77 - 326±2 353±2 347±2 146±13 571±64 442±49 245±37 -	0.04 - 350±26 - 953 1020 1004 271±7 910±35 720±27 424±20 -	W+C110 REF.	Scenarios Baseline_D B_EA Mix25_EA Mix50_EA Mix75_EA B_UA Mix25_UA Mix25_UA Mix50_UA Mix75_UA	0.01 - 186±987 -65±95 -64±90 -64±78 96±45 79±490 15±361 -43±256	0.02 - 234±251 - 30±21 37±20 36±16 226±15 232±140 164±105 64±77 -	0.03 - 284±78 - 259±5 281±5 276±3 403±8 453±64 346±50 184±37	0.04 - 322±27 - 767±1 820±1 808±1 647±5 725±35 569±27 328±20 -
W+C54 REF.	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA Mix75_EA B_UA Mix25_UA Mix50_UA Mix50_UA Mix75_UA B_EA Mix25_EA	0.01 - 199±957 - -74±44 -72±43 -72±37 -16±65 79±478 20±351 -40±244 - - -48±29	0.02 - 241±246 - 30±9 39±9 37±7 42±26 259±137 186±103 77±75 - 115±5	0.03 - 308±77 326±2 353±2 347±2 146±13 571±64 442±49 245±37 - 481±1	0.04 - 350±26 - 953 1020 1004 271±7 910±35 720±27 424±20 - 1312	REF.	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA Mix75_EA B_UA Mix25_UA Mix50_UA Mix50_UA Mix75_UA B_EA Mix25_EA	0.01 - 186±987 - -65±95 -64±90 -64±78 96±45 79±490 15±361 -43±256 - - -57±62	0.02 - 234±251 30±21 37±20 36±16 226±15 232±140 164±105 64±77 - 75±11	0.03 - 284±78 259±5 281±5 276±3 403±8 453±64 346±50 184±37 - 374±2	0.04 - 322±27 - 767±1 820±1 808±1 647±5 725±35 569±27 328±20 - 1009
W+C54 REF.	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA Mix75_EA Mix25_UA Mix25_UA Mix75_UA B_EA Mix25_EA Mix25_EA	0.01 - 199±957 - -74±44 -72±43 -72±37 -16±65 79±478 20±351 -40±244 - - -48±29 -3±369	0.02 - 241±246 - 30±9 39±9 37±7 42±26 259±137 186±103 77±75 - 115±5 -4±96	0.03 - 308±77 - 326±2 353±2 347±2 146±13 571±64 442±49 245±37 - 481±1 -4±32	0.04 - 350±26 - 953 1020 1004 271±7 910±35 720±27 424±20 - 1312 -1±12	W+C110 REF.	Scenarios Baseline_D B_EA Mix25_EA Mix50_EA Mix75_EA B_UA Mix25_UA Mix25_UA Mix75_UA B_EA Mix25_EA Mix25_EA	0.01 - 186±987 -65±95 -64±90 -64±78 96±45 79±490 15±361 -43±256 - -57±62 -5±373	0.02 - 234±251 30±21 37±20 36±16 226±15 232±140 164±105 64±77 - 75±11 -3±97	0.03 - 284±78 - 259±5 281±5 276±3 403±8 453±64 346±50 184±37 - 374±2 0±32	0.04 - 322±27 - 767±1 820±1 808±1 647±5 725±35 569±27 328±20 - 1009 0±12
W+C54 REF.	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA Mix75_EA B_UA Mix25_UA Mix50_UA Mix75_UA B_EA Mix25_EA Mix25_EA Mix50_EA	0.01 - 199±957 - 74±44 -72±43 -72±37 -16±65 79±478 20±351 -40±244 - - 40±244 - - 48±29 -3±369 -13±333	0.02 - 241±246 - 30±9 39±9 37±7 42±26 259±137 186±103 77±75 - 115±5 -4±96 -26±89	0.03 - 308±77 326±2 353±2 347±2 146±13 571±64 442±49 245±37 - 481±1 -4±32 -35±30	0.04 - 350±26 - 953 1020 1004 271±7 910±35 720±27 424±20 - 1312 -1±12 -40±11	REF. 8 5: 8 4: 2	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA Mix75_EA Mix25_UA Mix50_UA Mix50_UA B_EA Mix25_EA Mix25_EA Mix50_EA	0.01 - 186±987 - -65±95 -64±90 -64±78 96±45 79±490 15±361 -43±256 - - -57±62 -5±373 -29±336	0.02 - 234±251 30±21 37±20 36±16 226±15 232±140 164±105 64±77 - 75±11 -3±97 -39±89	0.03 - 284±78 259±5 281±5 276±3 403±8 453±64 346±50 184±37 - 374±2 0±32 -38±30	0.04 - 322±27 - 767±1 820±1 808±1 647±5 725±35 569±27 328±20 - 1009 0±12 -39±11
RCP 8.5 RCP 4.5	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA Mix75_EA Mix25_UA Mix50_UA Mix75_UA B_EA Mix25_EA Mix50_EA Mix75_EA B_UA	0.01 - 199±957 - -74±44 -72±43 -72±37 -16±65 79±478 20±351 -40±244 - - -48±29 -3±369 -13±333 39±66	0.02 - 241±246 - 30±9 39±9 37±7 42±26 259±137 186±103 77±75 - 115±5 -4±96 -26±89 93±27	0.03 - 308±77 - 326±2 353±2 347±2 146±13 571±64 442±49 245±37 - 481±1 -4±32 -35±30 178±14	0.04 - 350±26 - 953 1020 1004 271±7 910±35 720±27 424±20 - 1312 -1±12 -40±11 313±7	RCP 8.5 RCP 4.5	Scenarios Baseline_D B_EA Mix25_EA Mix50_EA Mix75_EA B_UA Mix25_UA Mix25_UA Mix75_UA Mix75_UA Mix25_EA Mix25_EA Mix25_EA Mix50_EA B_UA	0.01 - 186±987 -65±95 -64±90 -64±78 96±45 79±490 15±361 -43±256 - -57±62 -57±62 -5±373 -29±336 180±45	0.02 - 234±251 30±21 37±20 36±16 226±15 232±140 164±105 64±77 - 75±11 -3±97 -39±89 289±16	0.03 - 284±78 259±5 281±5 276±3 403±8 453±64 346±50 184±37 - 374±2 0±32 -38±30 461±8	0.04 - 322±27 - 767±1 820±1 808±1 647±5 725±35 569±27 328±20 - 1009 0±12 -39±11 700±5
RCP 8.5 RCP 4.5	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA B_UA Mix25_UA Mix25_UA Mix50_UA Mix75_UA B_EA Mix25_EA Mix50_EA Mix50_EA Mix75_EA B_UA	0.01 - 199±957 - 74±44 -72±43 -72±37 -16±65 79±478 20±351 -40±244 - - 40±244 - - 48±29 -3±369 -13±333 39±66 170±439	0.02 - 241±246 - 30±9 39±9 37±7 42±26 259±137 186±103 77±75 - 115±5 -4±96 -26±89 93±27 351±125	0.03 - 308±77 326±2 353±2 347±2 146±13 571±64 442±49 245±37 - 481±1 -4±32 -35±30 178±14 622±59	0.04 - 350±26 - 953 1020 1004 271±7 910±35 720±27 424±20 - 1312 -1±12 -40±11 313±7 991±32	RCP 8.5 RCP 4.5	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA Mix75_EA Mix25_UA Mix50_UA Mix75_UA Mix25_UA Mix25_EA Mix25_EA Mix50_EA Mix75_EA B_UA Mix25_UA	0.01 - 186±987 - -65±95 -64±90 -64±78 96±45 79±490 15±361 -43±256 - - -57±62 -5±373 -29±336 180±45 138±452	0.02 - 234±251 30±21 37±20 36±16 226±15 232±140 164±105 64±77 - 75±11 -3±97 -39±89 289±16 266±128	0.03 - 284±78 259±5 281±5 276±3 403±8 453±64 346±50 184±37 - 374±2 0±32 -38±30 461±8 488±59	0.04 - 322±27 - 767±1 820±1 808±1 647±5 725±35 569±27 328±20 - 1009 0±12 -39±11 700±5 757±32
RCP 8.5 RCP 4.5	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA Mix75_EA B_UA Mix25_UA Mix50_UA Mix25_EA Mix25_EA Mix50_EA Mix75_EA B_UA Mix25_UA Mix25_UA	0.01 - 199±957 - -74±44 -72±43 -72±37 -16±65 79±478 20±351 -40±244 - - -48±29 -3±369 -13±333 39±66 170±439 63±351	0.02 - 241±246 - 30±9 39±9 37±7 42±26 259±137 186±103 77±75 - 115±5 -4±96 -26±89 93±27 351±125 257±102	0.03 - 308±77 - 326±2 353±2 347±2 146±13 571±64 442±49 245±37 - 481±1 -4±32 -35±30 178±14 622±59 483±49	0.04 - 350±26 - 953 1020 1004 271±7 910±35 720±27 424±20 - 1312 -1±12 -40±11 313±7 991±32 788±26	RCP 8.5 RCP 4.5	Scenarios Baseline_B Baseline_O B_EA Mix25_EA Mix50_EA Mix75_EA Mix25_UA Mix50_UA Mix75_UA Mix25_EA Mix50_EA Mix75_EA B_UA Mix25_UA Mix25_UA	0.01 - 186±987 - -65±95 -64±90 -64±78 96±45 79±490 15±361 -43±256 - - 57±62 - 5±373 -29±336 180±45 138±452 40±362	$\begin{array}{c} \textbf{0.02} \\ \hline \\ 234 \pm 251 \\ \hline \\ 30 \pm 21 \\ 37 \pm 20 \\ 36 \pm 16 \\ 226 \pm 15 \\ 232 \pm 140 \\ 164 \pm 105 \\ 64 \pm 77 \\ \hline \\ 75 \pm 11 \\ -3 \pm 97 \\ -39 \pm 89 \\ 289 \pm 16 \\ 266 \pm 128 \\ 190 \pm 104 \\ \end{array}$	0.03 - 284±78 259±5 281±5 276±3 403±8 453±64 346±50 184±37 - 374±2 0±32 -38±30 461±8 488±59 375±49	0.04 - 322±27 - 767±1 820±1 808±1 647±5 725±35 569±27 328±20 - 1009 0±12 -39±11 700±5 757±32 598±26

#### 7 Synergy analysis of adaptation strategies

From an economic perspective, the combination of different strategies (or species) can be more beneficial for the forest owner than each strategy (species) separately, i.e., synergies between adaptation strategies (or species) can appear. According to Pretzsch and Schütze [10], two levels of synergies exist.

First, overyielding is defined as a higher observed parameter  $P_{mix}$  in the mixed stand than the expected parameter  $P_{mix}$  [10], i.e.,

$$P_{mix} > P_{mix} \leftrightarrow P_{mix} > q_1 \cdot P_1 + q_2 \cdot P_2$$

where  $q_1$  and  $q_2$  are the respective mixing proportions of species 1 and species 2, and  $P_1$  and  $P_2$  the respective parameter of species 1 and species 2 in a monoculture stand.

Transgressive overyielding of the mixed stand can then be observed, when the observed parameter  $P_{mix}$  is higher than the parameter of both species in a monoculture stand ( $P_1$  and  $P_2$ ) [10], i.e.,

$$P_{mix} > P_1$$
 and  $P_{mix} > P_2$ 

The tested parameters were the total volume harvested and the land expectation value. In order to test the presence of synergies, even-aged and uneven-aged oak stands were simulated. The results are presented in Tables 7 and 8. Overyielding is represented by a coefficient of 1 and transgressive overyielding by a coefficient of 1+. An absence of overyielding is represented by a coefficient of 0.

**Table 7** Results of the tested synergy of mixed stands in terms of total volume harvested characterized by overyielding (coefficient 1) or transgressive overyielding (coefficient 1+) or absence (coefficient 0) for each scenario and considering four discount rates (1%, 2%, 3% and 4%)

Scenario		0.01	0.02	0.03	0.04
	B_EA	-	-	-	-
	Mix25_EA	0	0	0	1
	Mix50_EA	0	0	1+	1+
	Mix75_EA	0	0	1+	1+
KCP 4.5	B_UA	0	0	1+	1+
	Mix25_UA	0	1	0	0
	Mix50_UA	0	1	0	0
	Mix75_UA	0	0	0	0
	B_EA	-	-	-	-
	Mix25_EA	1+	1+	1+	1+
	Mix50_EA	1+	1+	1+	0
	Mix75_EA	1+	1+	1+	1+
RCP 8.5	B_UA	0	0	0	0
	Mix25_UA	0	1	1	1
	Mix50_UA	0	1	1	1
	Mix75_UA	0	1	1	1

**Table 8** Results of the tested synergy of mixed stands in terms of LEV considering only timber production (W) or with carbon storage for a carbon value of 28 EUR/tC, 54 EUR/tC and 110 EUR/tC, characterized by overyielding (coefficient 1) or transgressive overyielding (coefficient 1+) or absence (coefficient 0) for each scenario and considering four discount rates (1%, 2%, 3% and 4%)

			0	.01			0.	.02			0.	.03			0	.04	
Scenario		W	28	54	110	W	28	54	110	W	28	54	110	W	28	54	110
	B_EA	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	Mix25_EA	0	0	0	0	0	0	0	0	1	1	1	0	1+	1+	1+	1+
	Mix50_EA	0	0	0	0	0	0	0	0	1	1	1	1	1+	1+	1+	1+
RCP	Mix75_EA	0	0	0	0	0	0	0	0	1	1	1	1	1+	1+	1+	1+
4.5	B_UA	0	0	0	0	0	0	0	1	1	1	1	1+	1	1	1	1+
	Mix25_UA	0	0	0	0	0	0	0	0	1	1	1	1	1	1	1	1
	Mix50_UA	0	0	0	0	1	1	0	0	1	1	1	1	1	1	1	1
	Mix75_UA	0	0	0	0	0	0	0	0	1	1	1	0	1	1	1	0
	B_EA	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	Mix25_EA	0	0	0	0	0	0	0	0	1+	1+	1+	1+	1+	1+	1+	1+
	Mix50_EA	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
RCP	Mix75_EA	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8.5	B_UA	0	0	0	1	0	0	0	1	1	1	1	1+	1	1	1	1+
	Mix25_UA	0	0	0	0	1	1	1	0	1	1	1	1	1	1	1	1
	Mix50_UA	0	0	0	0	1	1	1	1	1	1	1	1	1	1	1	1
	Mix75_UA	0	0	0	0	0	0	0	0	1	1	1	0	1	1	1	0

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